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Diagnosing Turbulence in the Tokamak Divertor

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Senior Consultant – Fusion

BOUT++ Workshop – 09/01/2023

SYSTEMS • ENGINEERING • TECHNOLOGY

Acknowledgement



UK Atomic Energy Authority

The vast majority work described within this presentation was undertaken whilst working for the UKAEA funded by EPSRC and EUROfusion – my thanks to all of my friends, collaborators, and colleagues who contributed to this work during that time

Open slide master and add classification here

What is divertor turbulence, and why is it important?

Can we *understand* divertor turbulence?

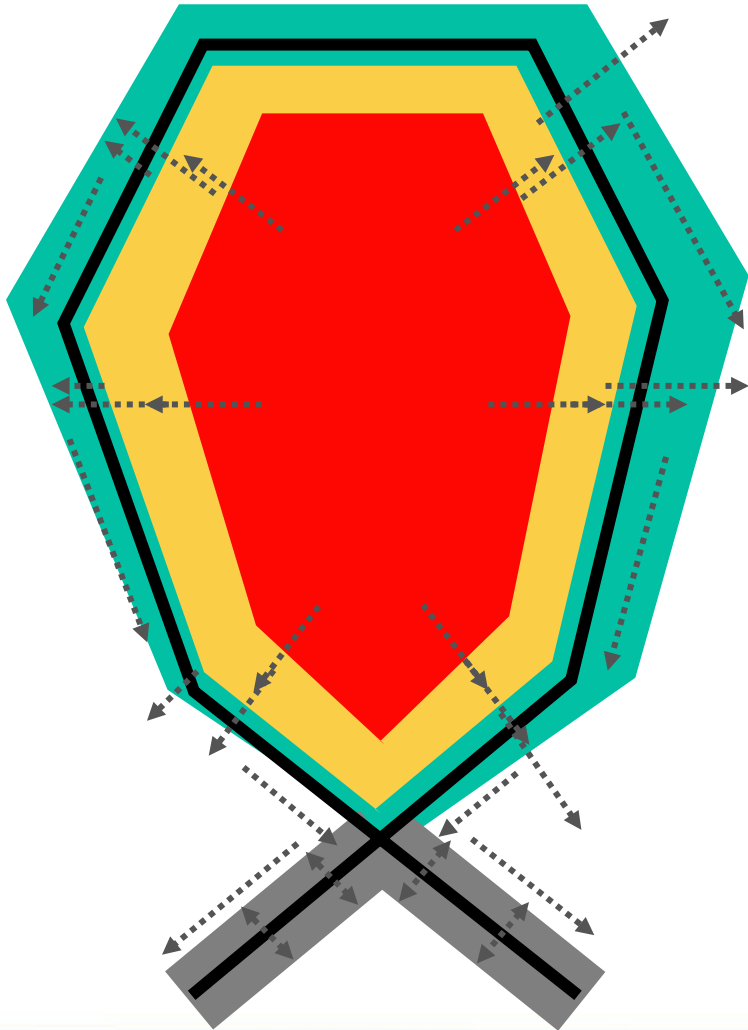
Summary

What is divertor turbulence, and why is it important?

Can we understand divertor turbulence?

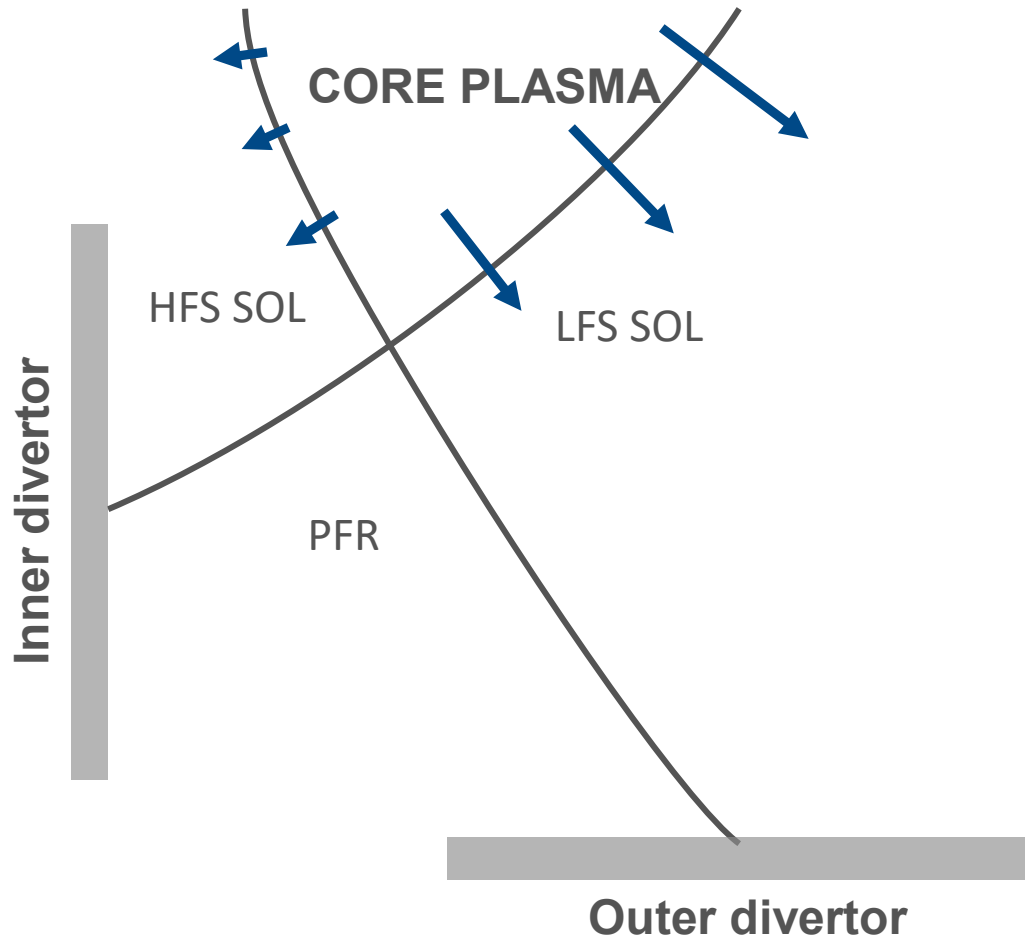
Summary

A 'Cubists' view of heat transport



- Well established physics basis**
- Core turbulence moves heat toward the edge determining the core pressure
 - Pedestal turbulence moves heat towards the separatrix determining the pedestal characteristics
 - Edge/Scrape-off layer turbulence moves heat onto open field lines determining the SOL width
 - **Divertor turbulence re-distributes heat in the divertor legs impacting deposition on the divertor target**

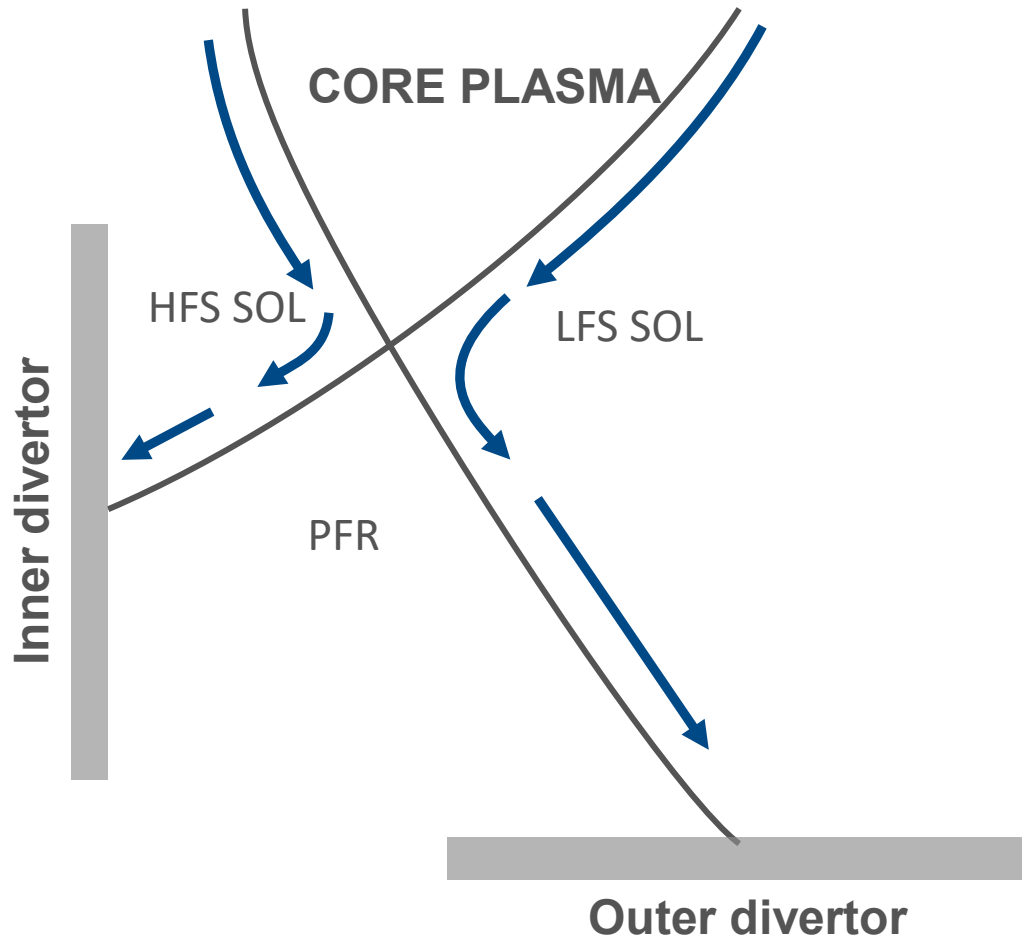
Importance of divertor transport



Transport processes that impact the divertor:

- Cross-field transport from the core into the scrape-off layer

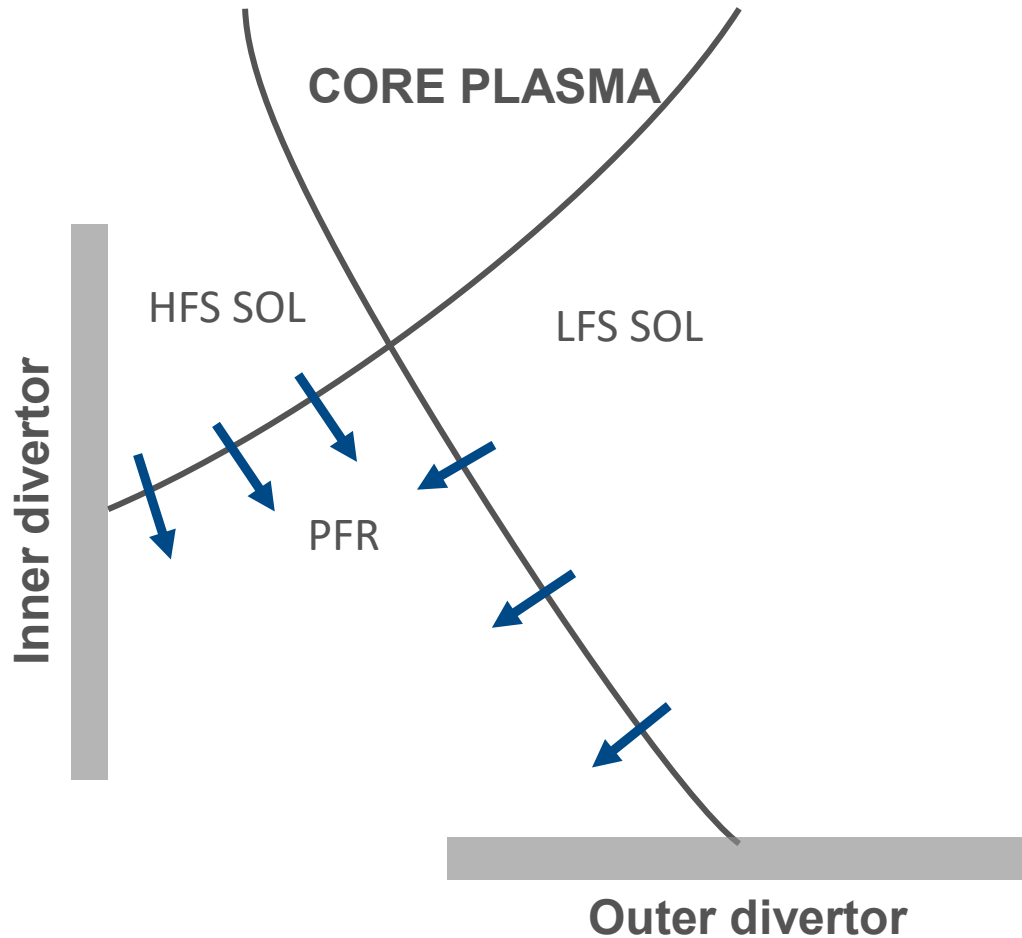
Importance of divertor transport



Transport processes that impact the divertor:

- Cross-field transport from the core into the scrape-off layer
- Parallel transport towards the divertor plates

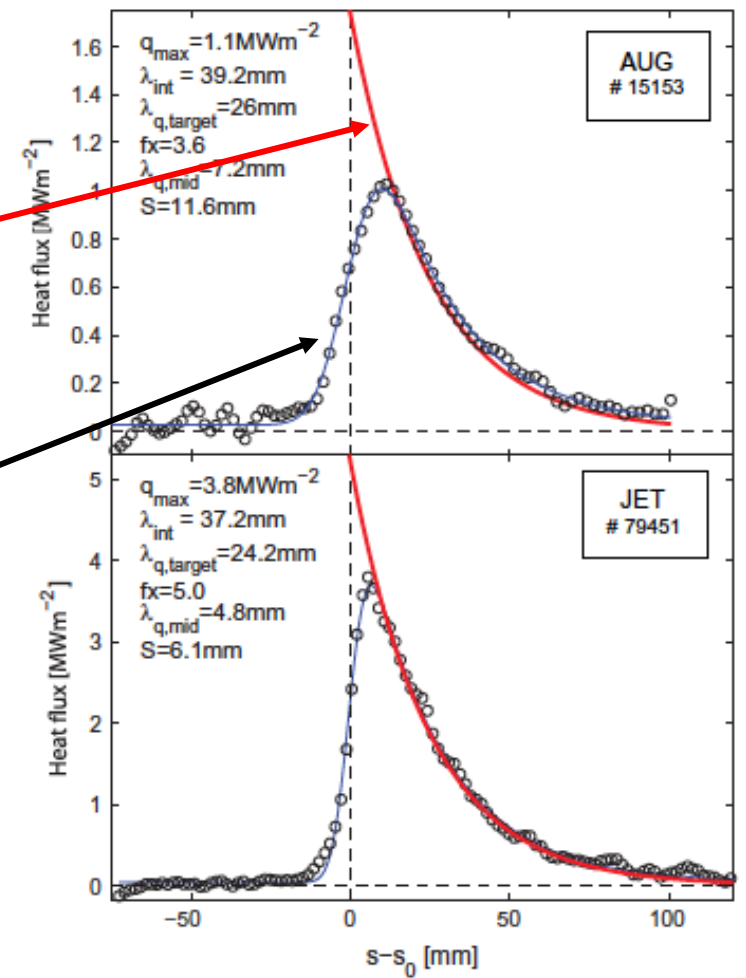
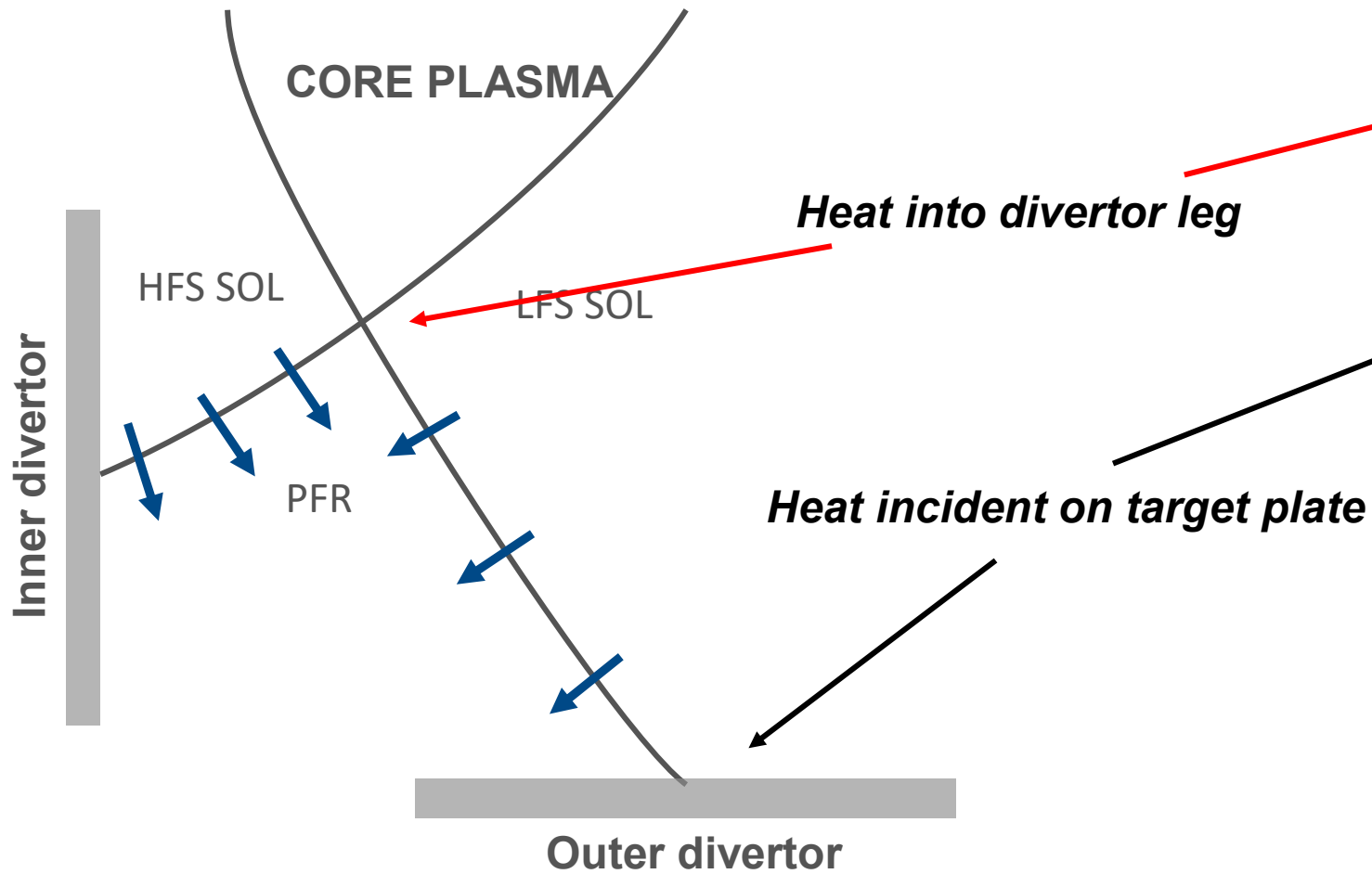
Importance of divertor transport



Transport processes that impact the divertor:

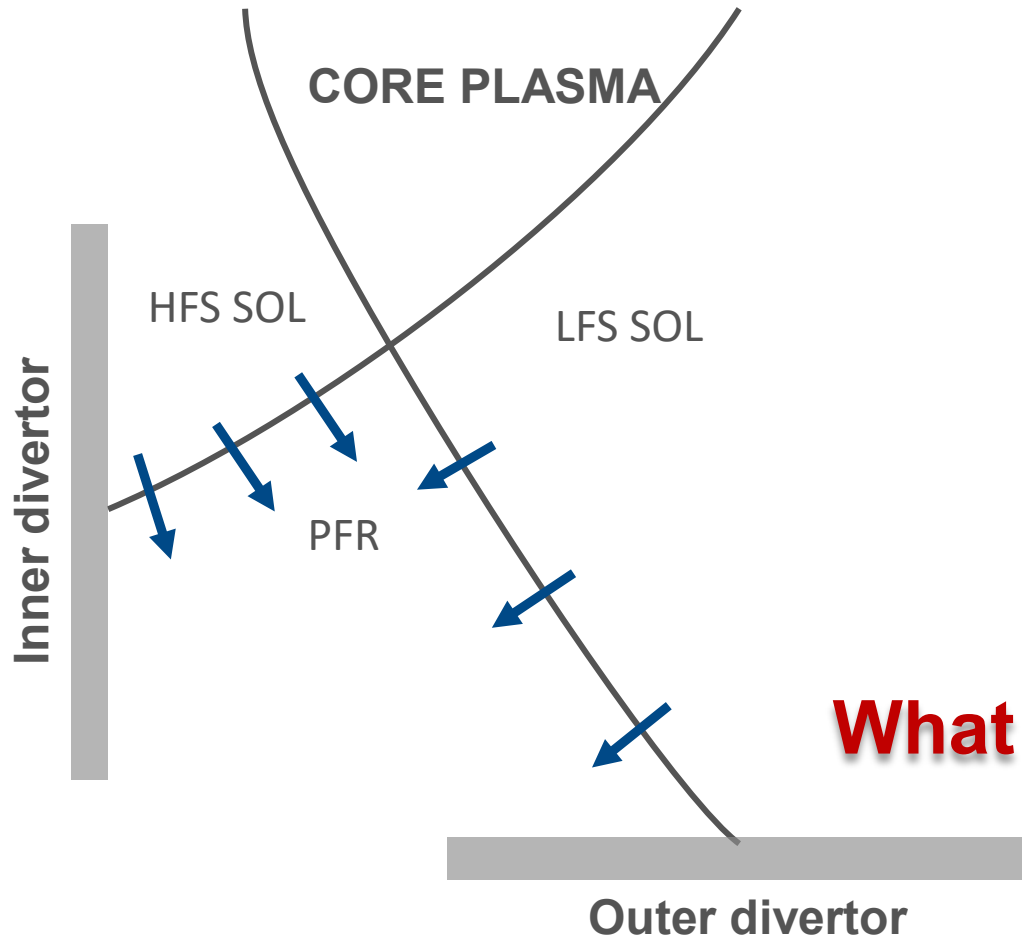
- Cross-field transport from the core into the scrape-off layer
- Parallel transport towards the divertor plates
- **Cross-field transport from the SOL into the PFR**

Importance of divertor transport



A. Scarabosio et al, JNM 57 (2017) 126028

Importance of divertor transport

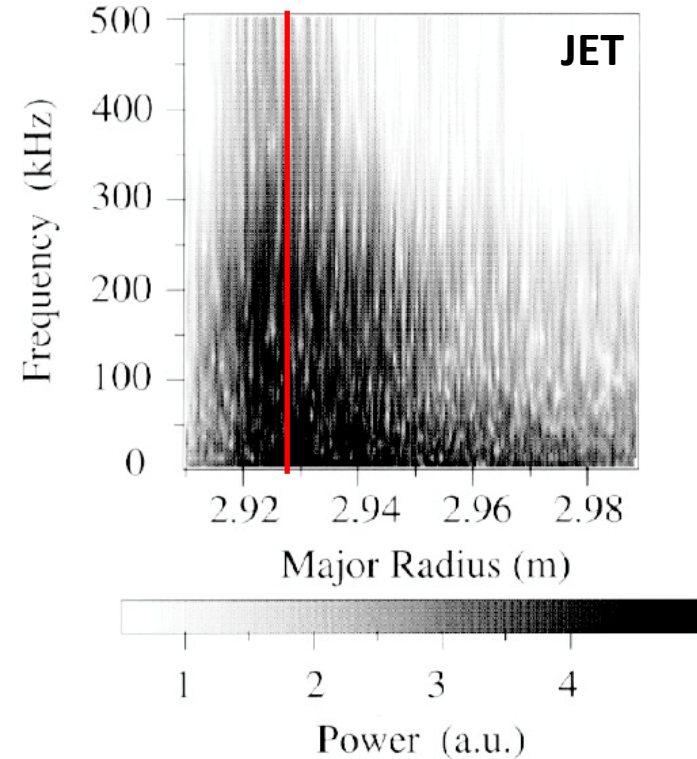


Divertor transport affects:

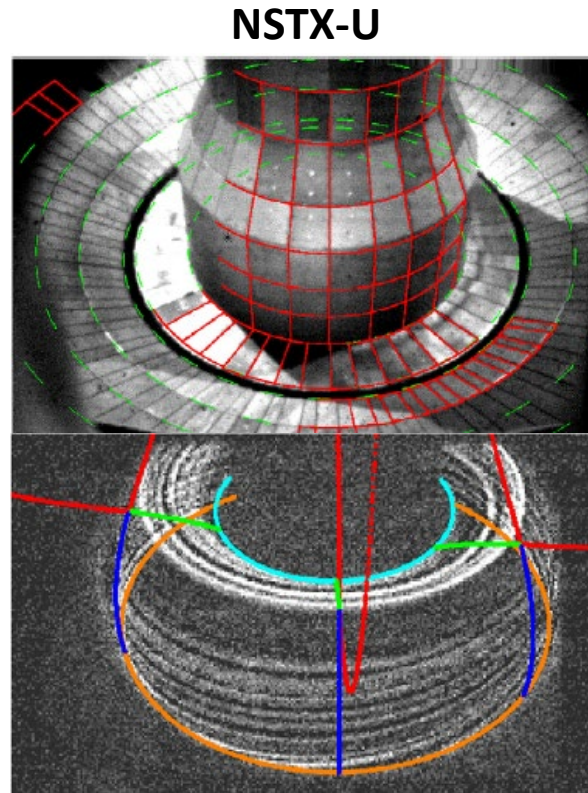
- The peak steady-state power hitting the divertor plate
- Detachment onset
- Helium pumping
- Peak ion temperature at the divertor

What is the origin of divertor transport?

Overview of observations around the world



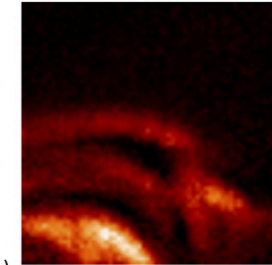
I.Garca-Cortes et al, PPCF 38 (1996) 2051



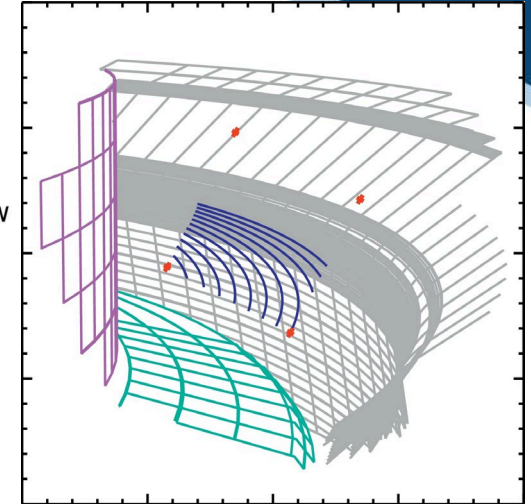
F.Scotti et al, NF 58 (2018) 126028

Alcator C-Mod

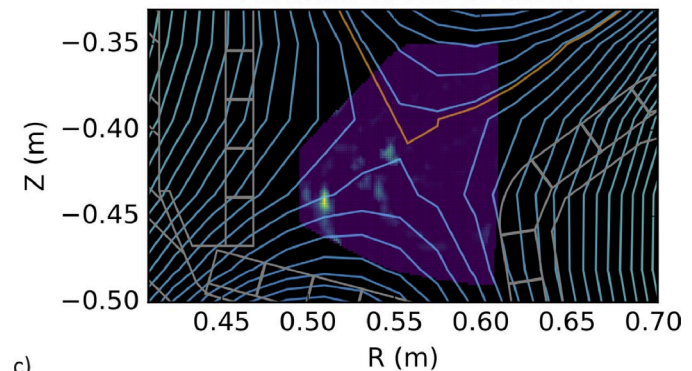
Divertor camera view



a)



Toroidal cross section

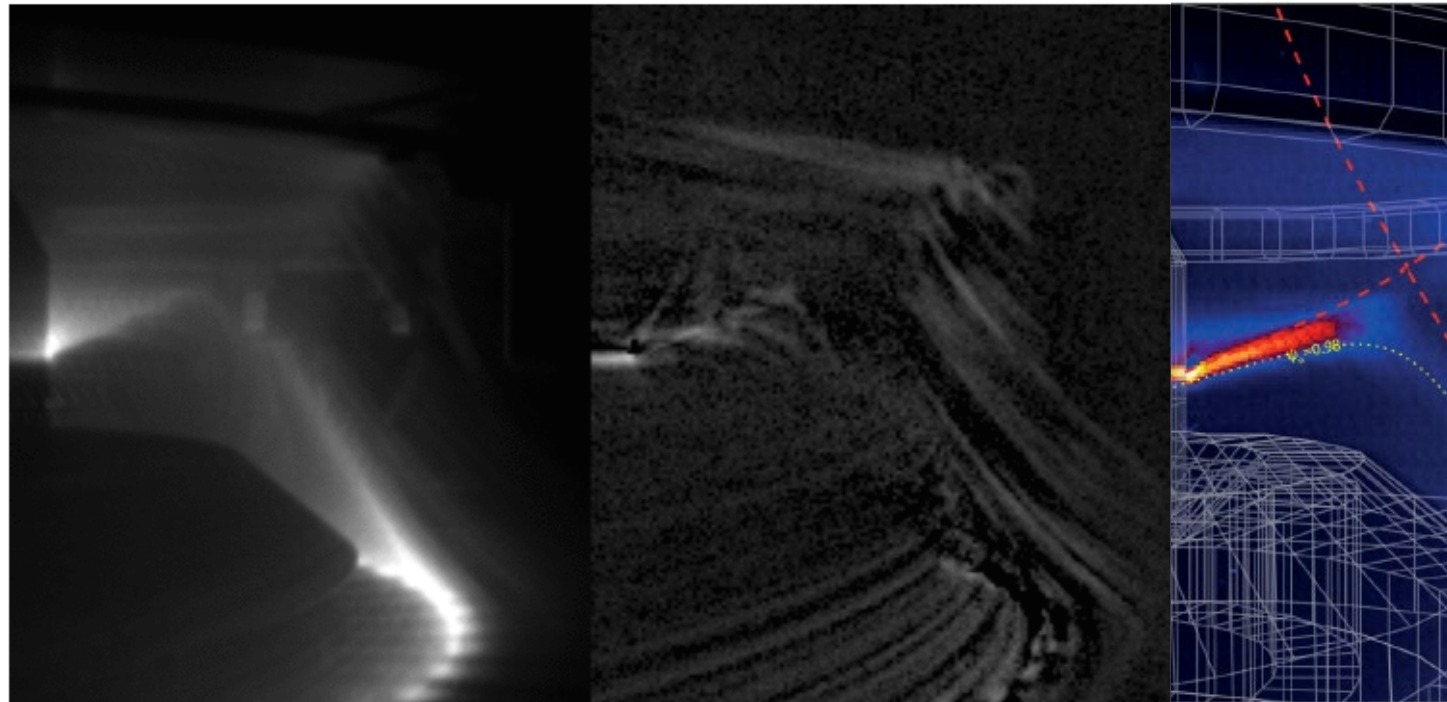


c)

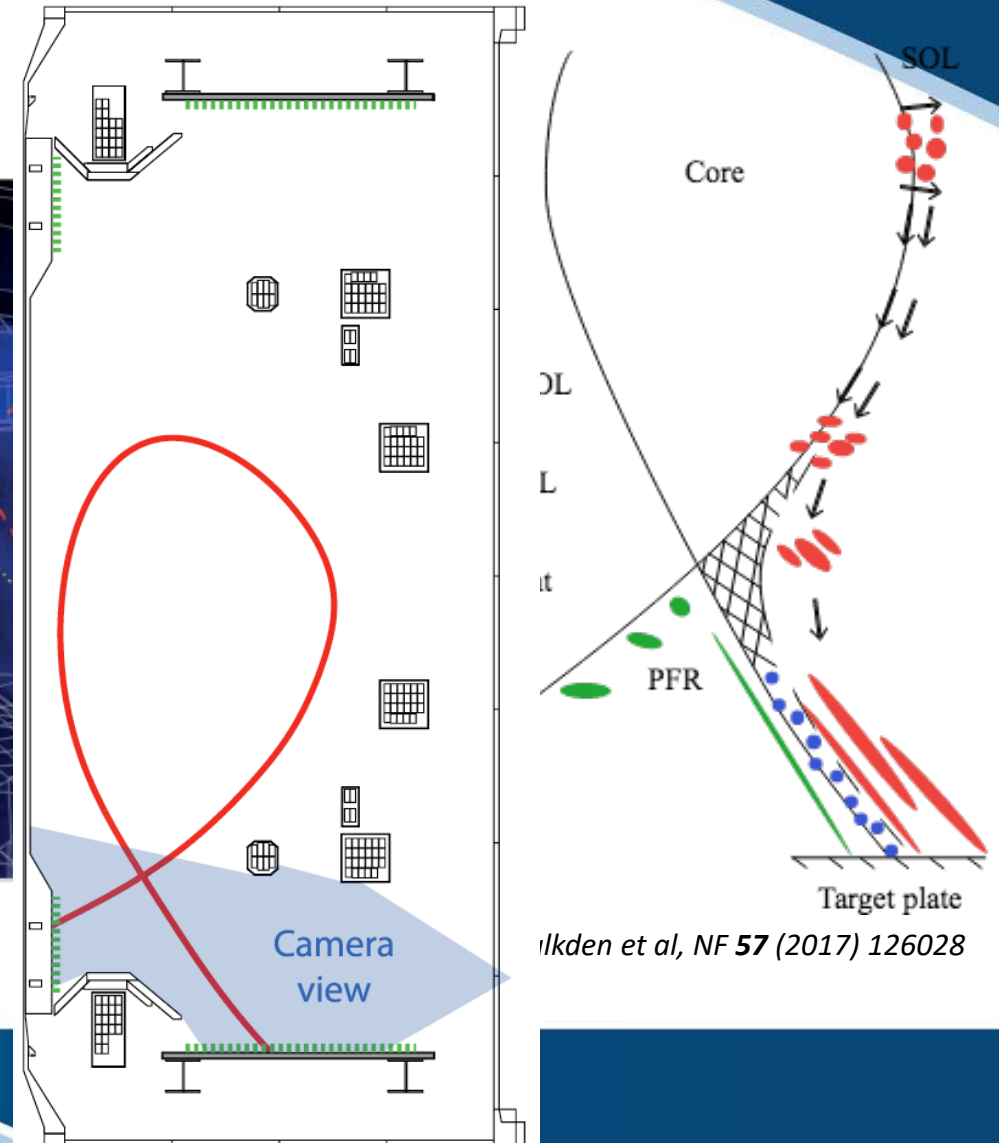
S.Ballinger et al, NME 17 (2018) 269

Overview of observations around the world

MAST



J.Harrison et al, PoP 22 (2015) 092508

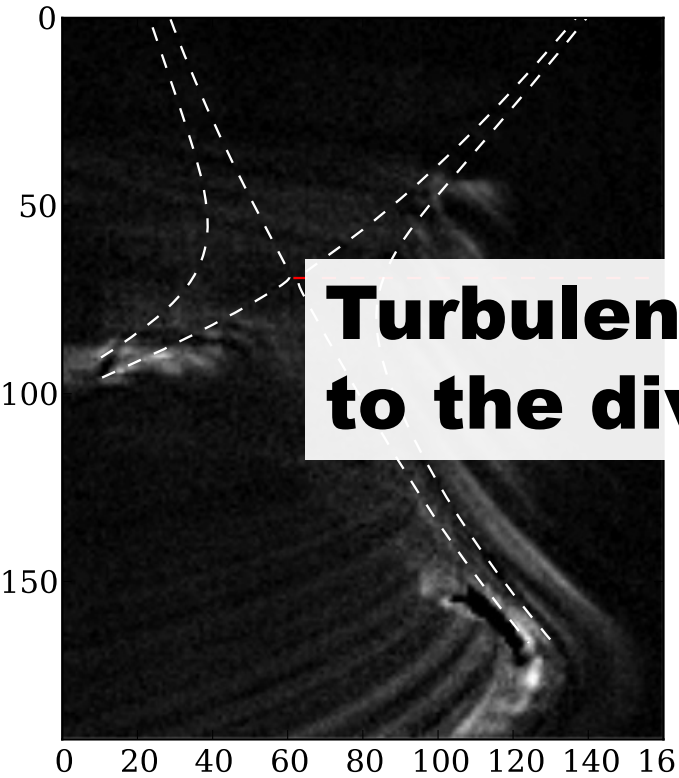


Ilkden et al, NF 57 (2017) 126028

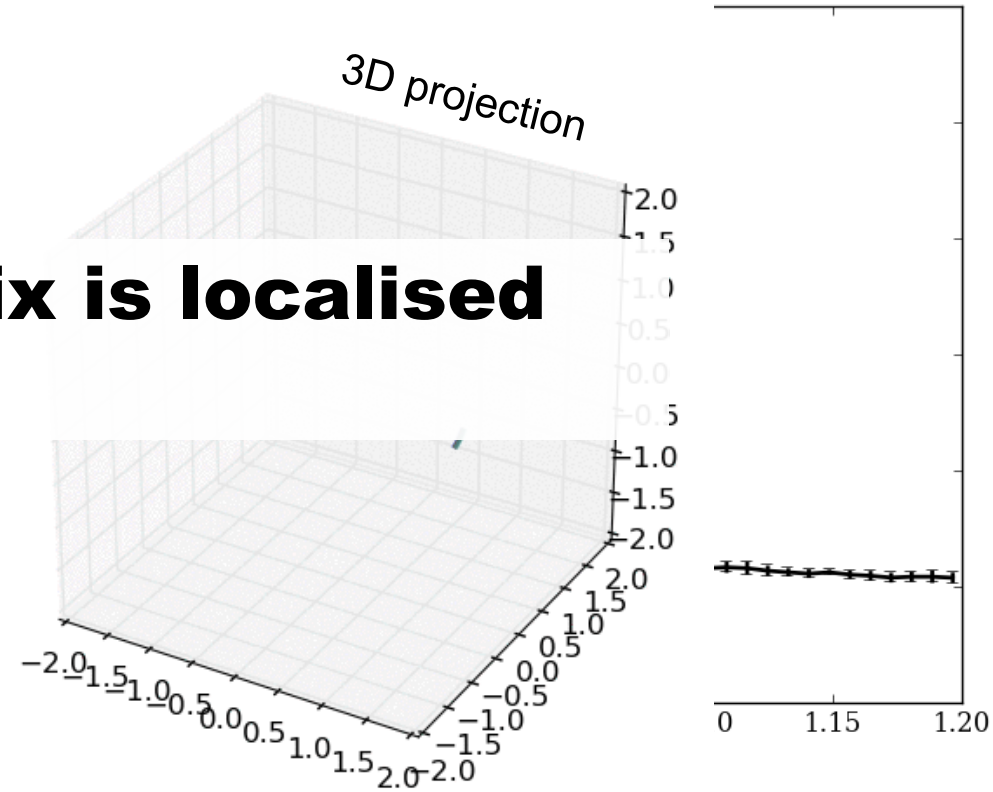
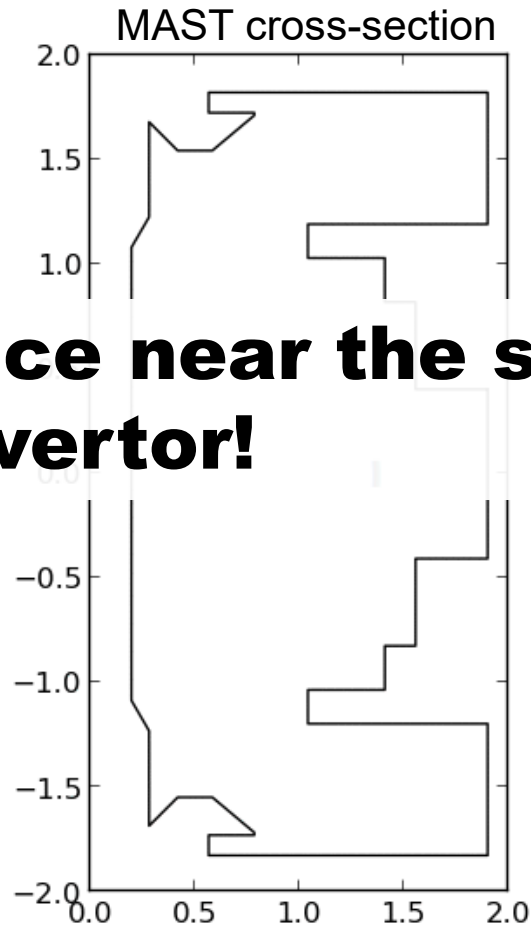
Effect of the X-point

Near the X-point, fluctuations from upstream are unable to enter the divertor

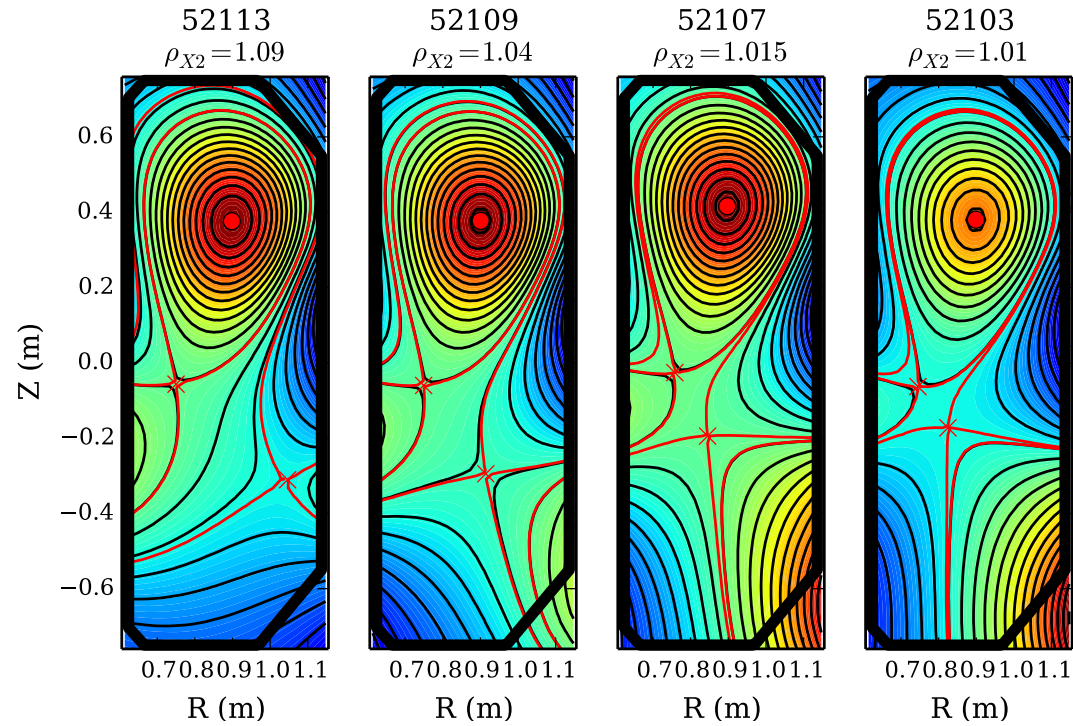
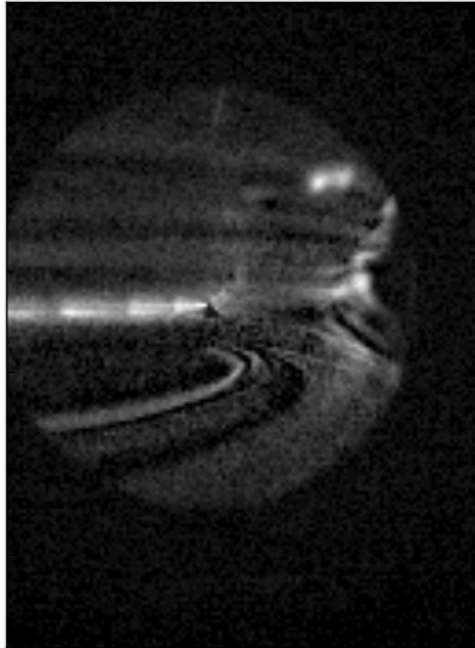
Turbulence near the separatrix is localised to the divertor!



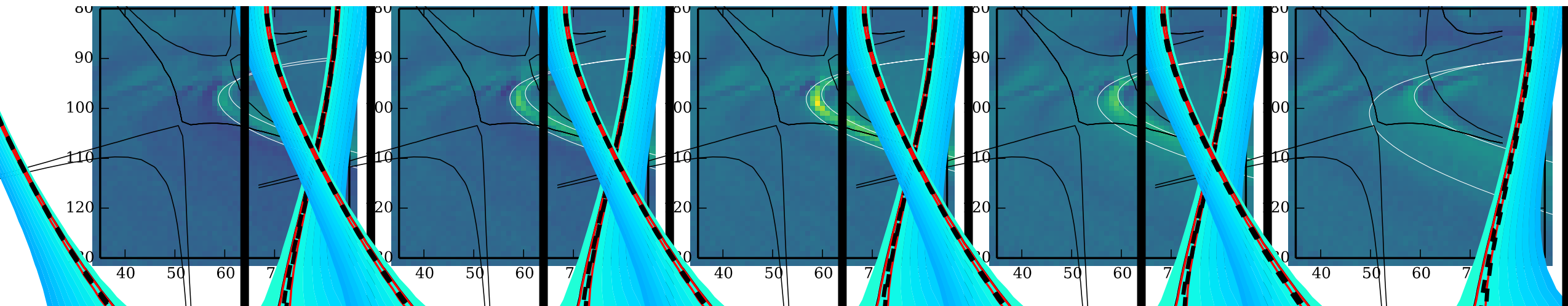
N.R.Walkden et al, NME 12 (2017) 175
N.R.Walkden et al, NF 57 (2017) 126028



Example from TCV snowflake plasmas



N.R.Walkden et al, PPCF 60 (2018) 115008



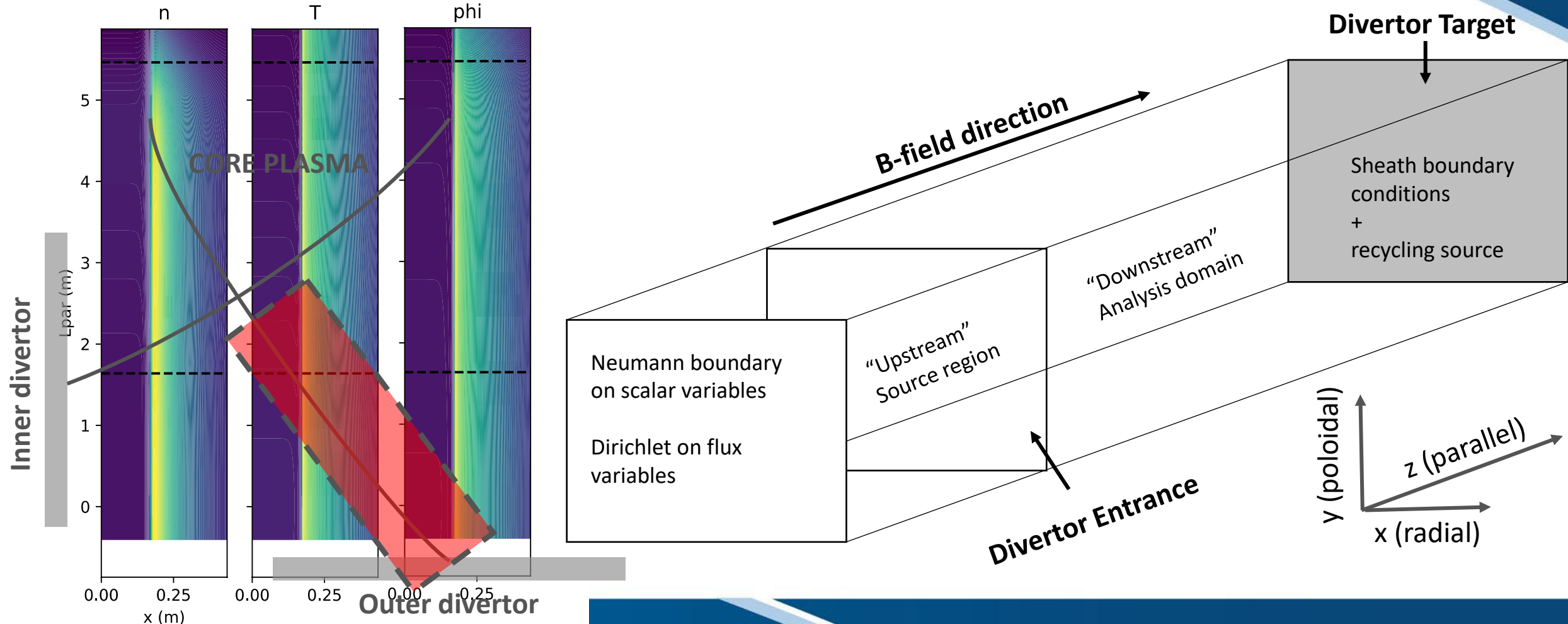
What is divertor turbulence, and why is it important?

Can we *understand* divertor turbulence?

Summary

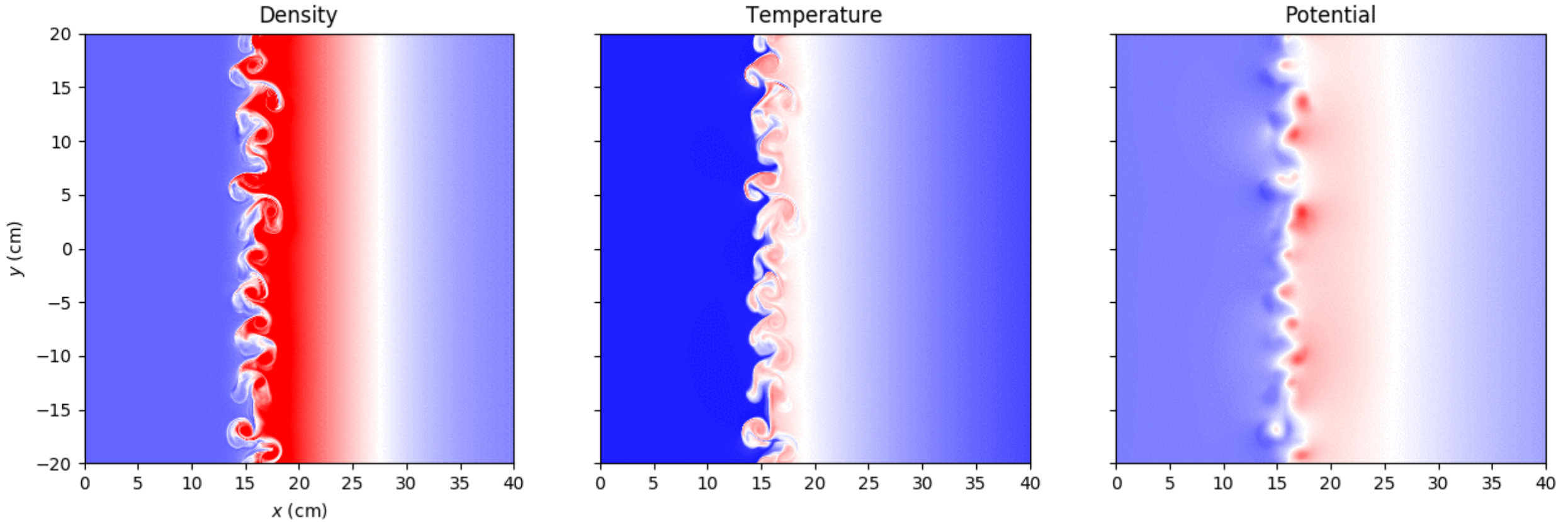
STEP 1: 'Mock-Divertor' slab simulations

For a first non-linear study, try to minimize the complexity to aid understanding
 → Simple slab representation of a single, isolated divertor leg

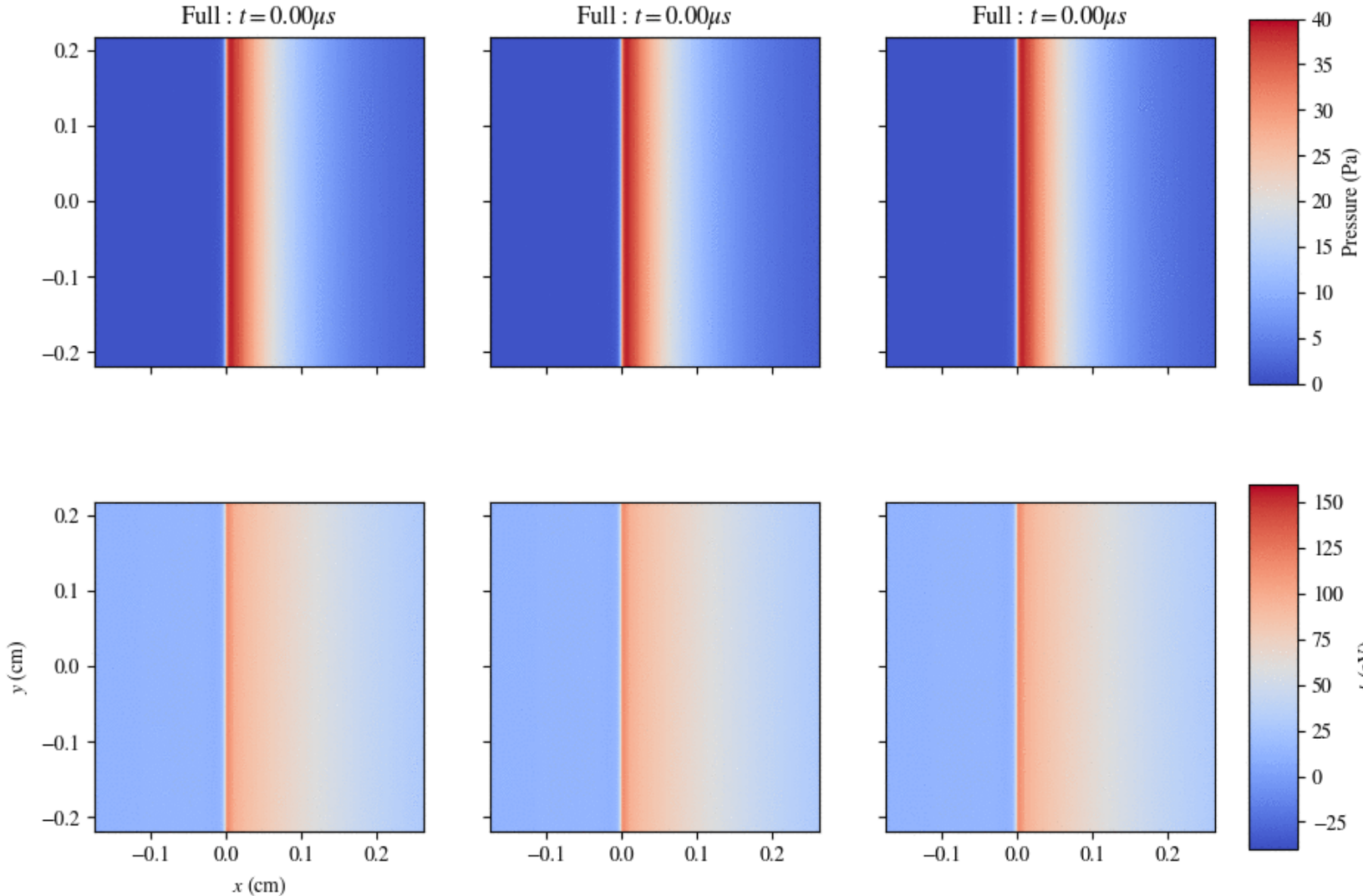


STEP 1: 'Mock-Divertor' slab simulations

Turbulence quickly develops in the vicinity of the separatrix



STEP 1: 'Mock-Divertor' slab simulations



By removing different driving terms we can isolate their effects

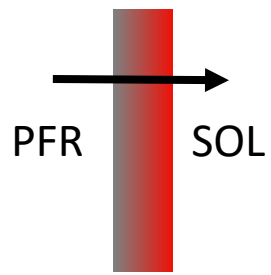
→ K-H turbulence responsible for driving the system

→ Curvature effects seem to play a regulatory role on the turbulence

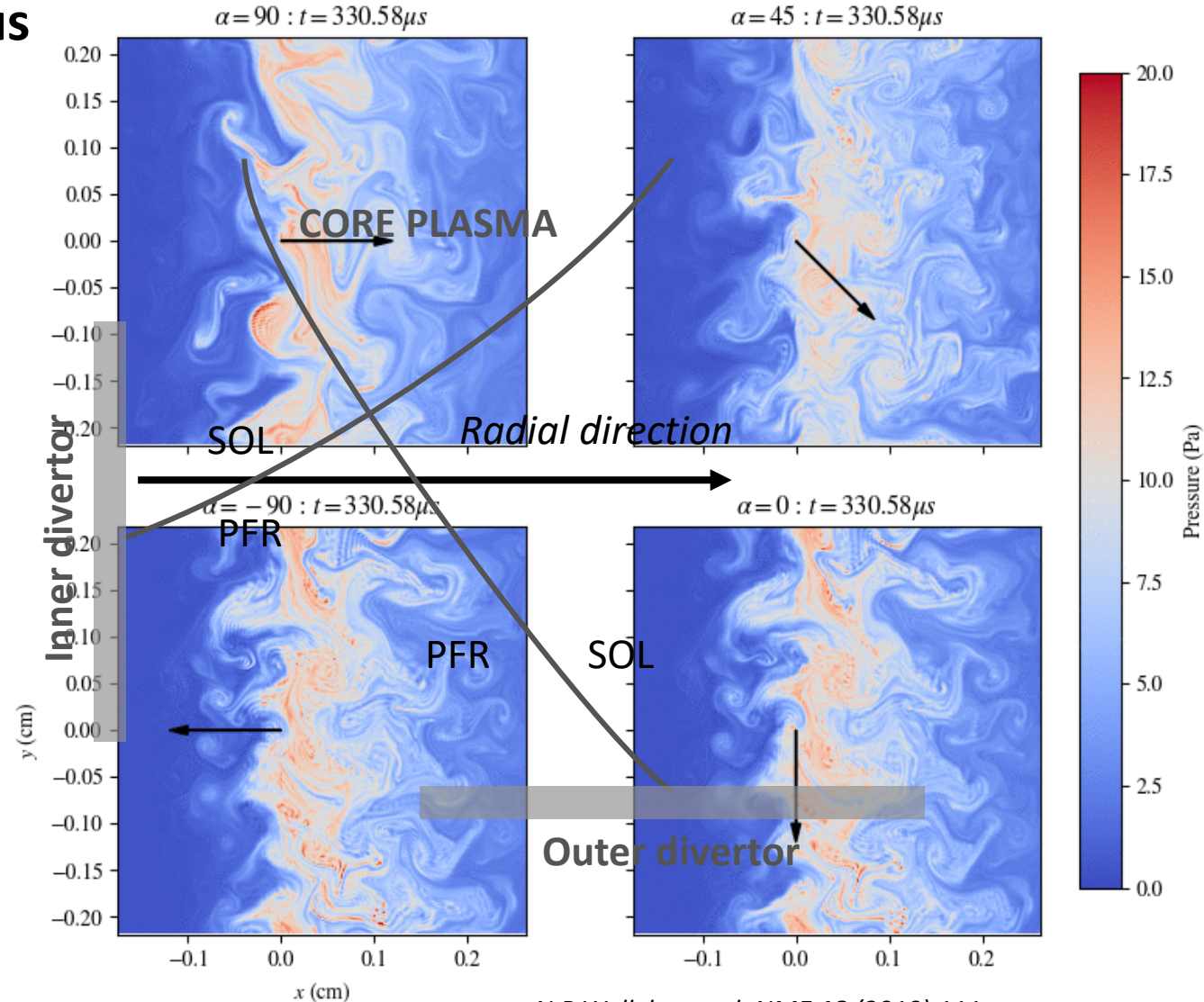
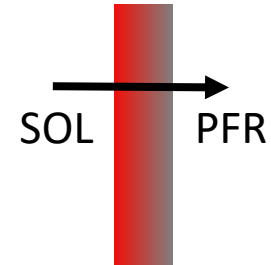
STEP 1: 'Mock-Divertor' slab simulations

In a tokamak magnetic curvature tends to force structures in the direction of the major radius

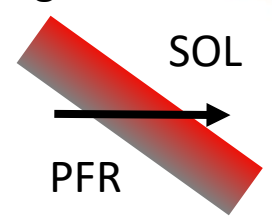
Vertical outer



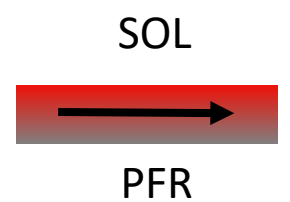
Vertical inner



Angled outer

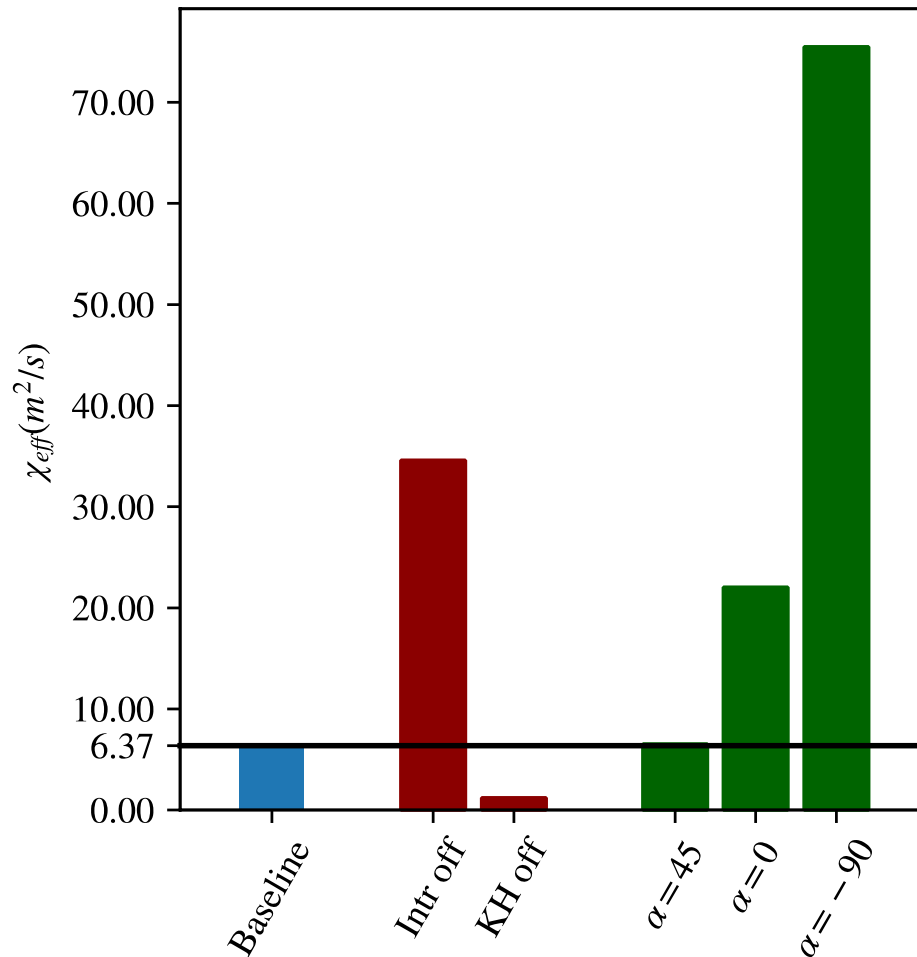


Horizontal outer



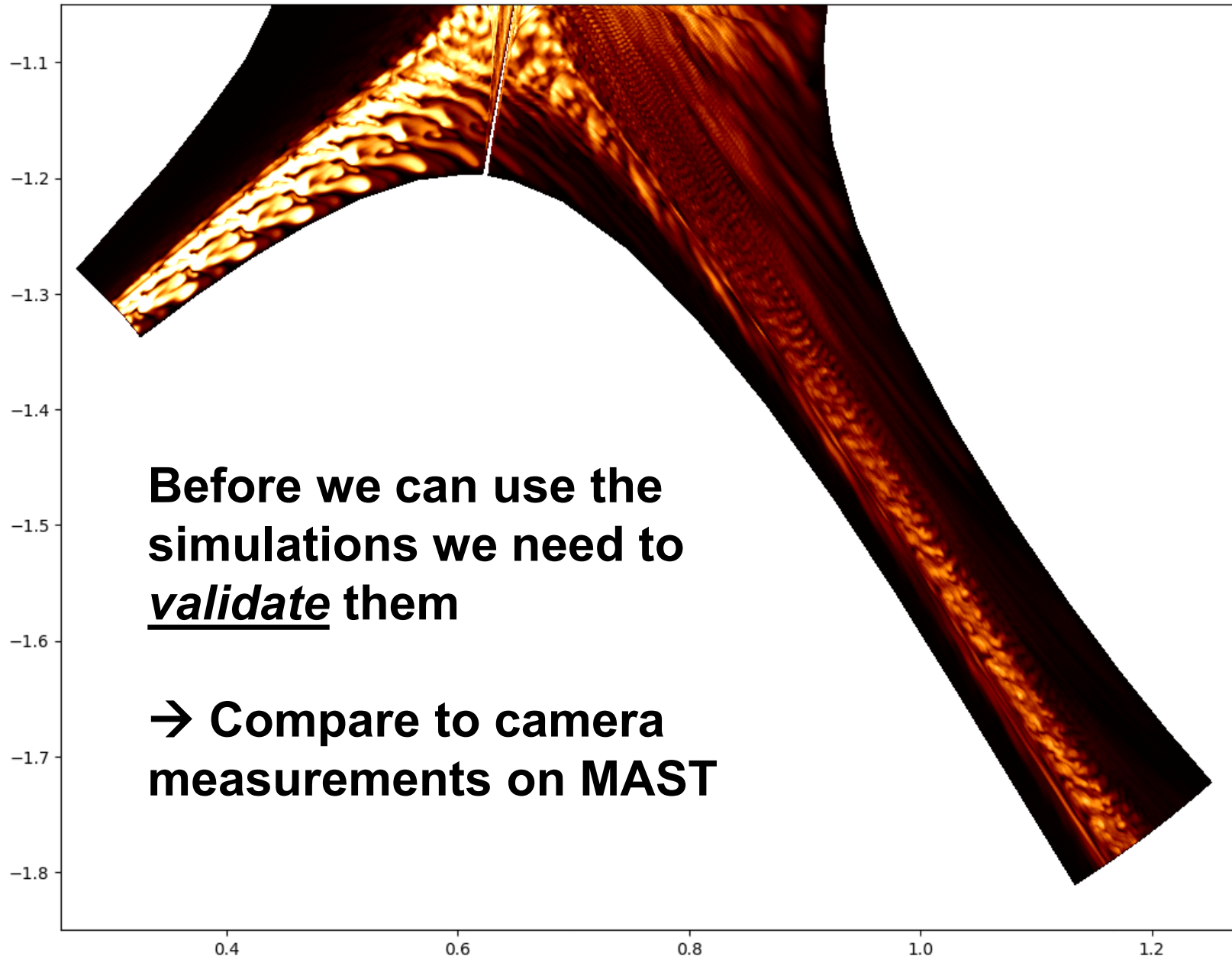
STEP 1: 'Mock-Divertor' slab simulations

In a tokamak magnetic curvature tends to force structures in the direction of the major radius



- The magnetic curvature is a principle actuator to vary the spreading parameter
- Other factors appear to have a minimal effect
- This is due to the balance between perpendicular and parallel transport

STEP 2: Validate full geometry simulations

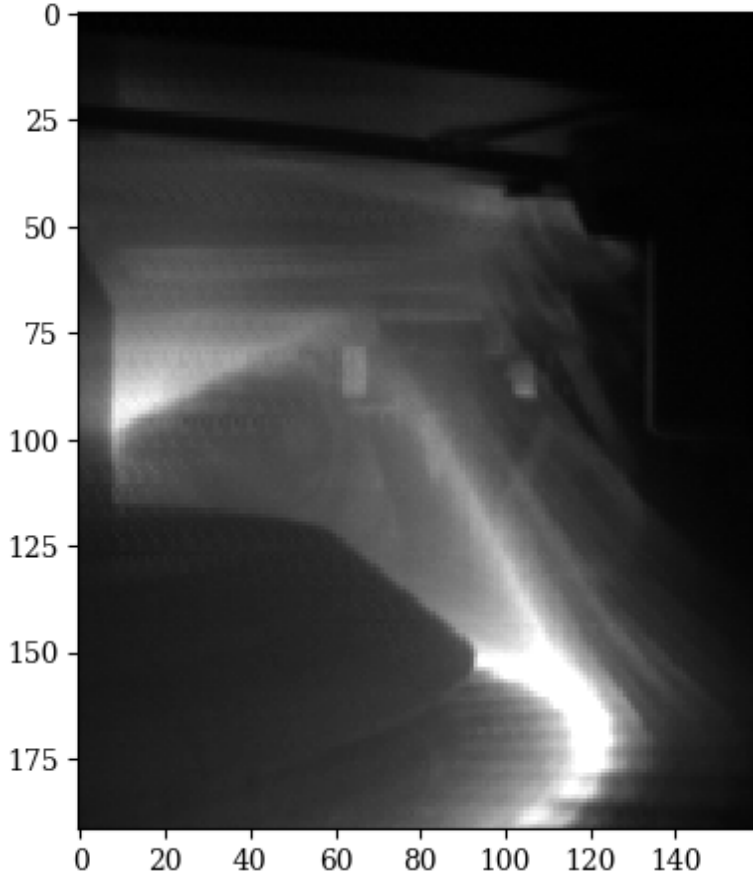


F.Riva *et al* Plasma Phys. Control. Fusion **61** (2019) 094013

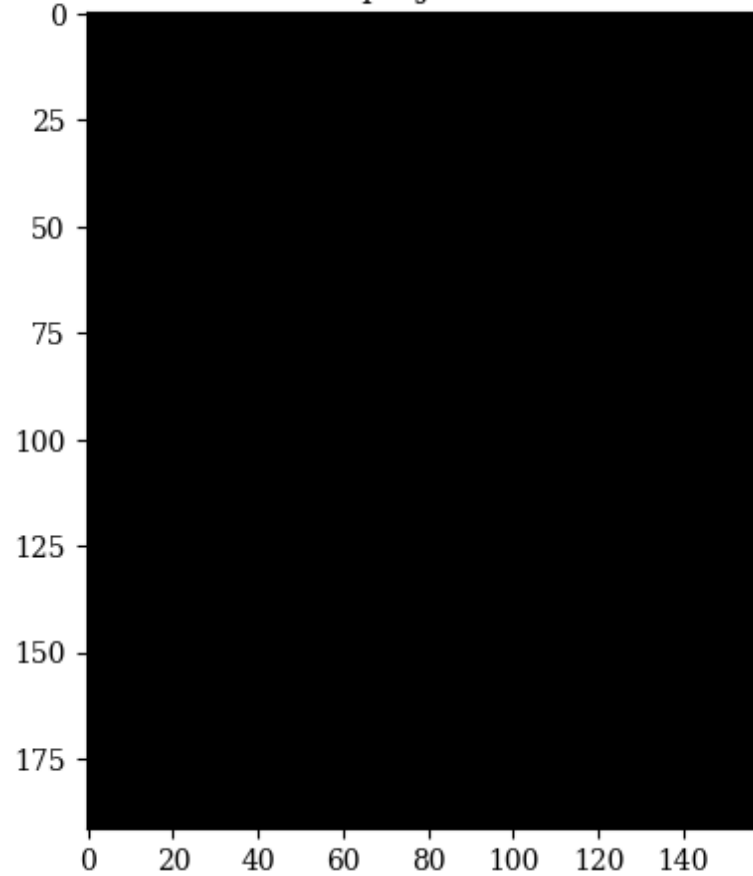
STEP 2: Validate full geometry simulations

Goal: Extract properties of fluctuating structures in real space from camera images

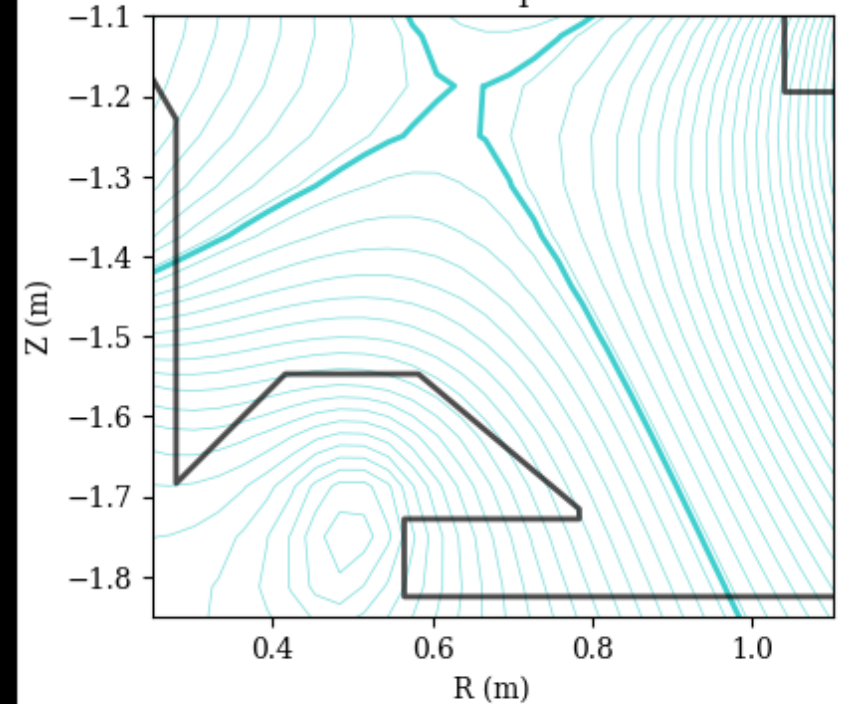
Camera frame



Reprojection



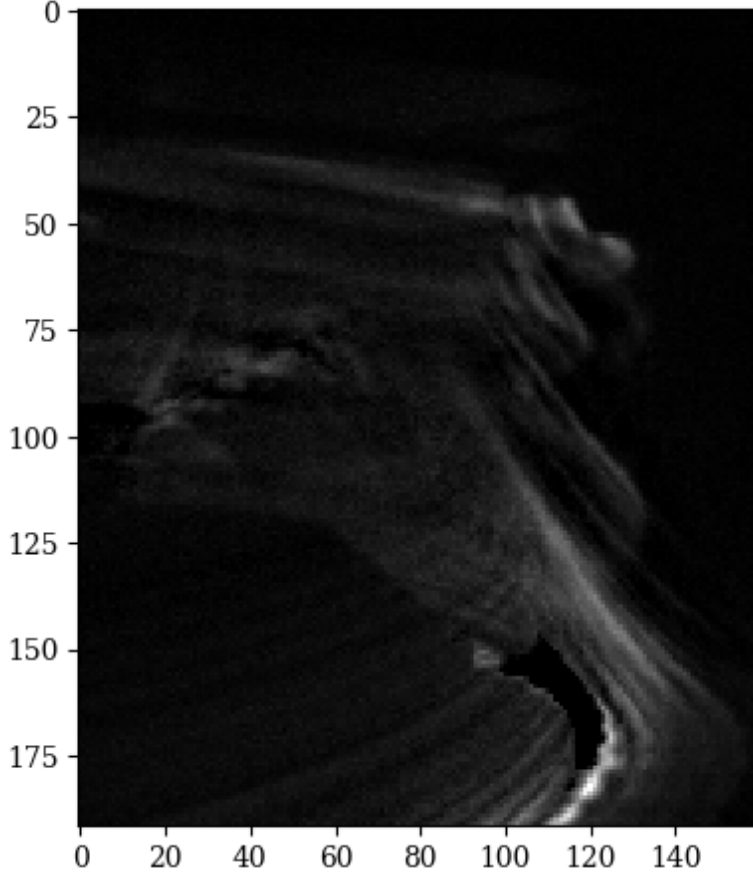
Poloidal plane



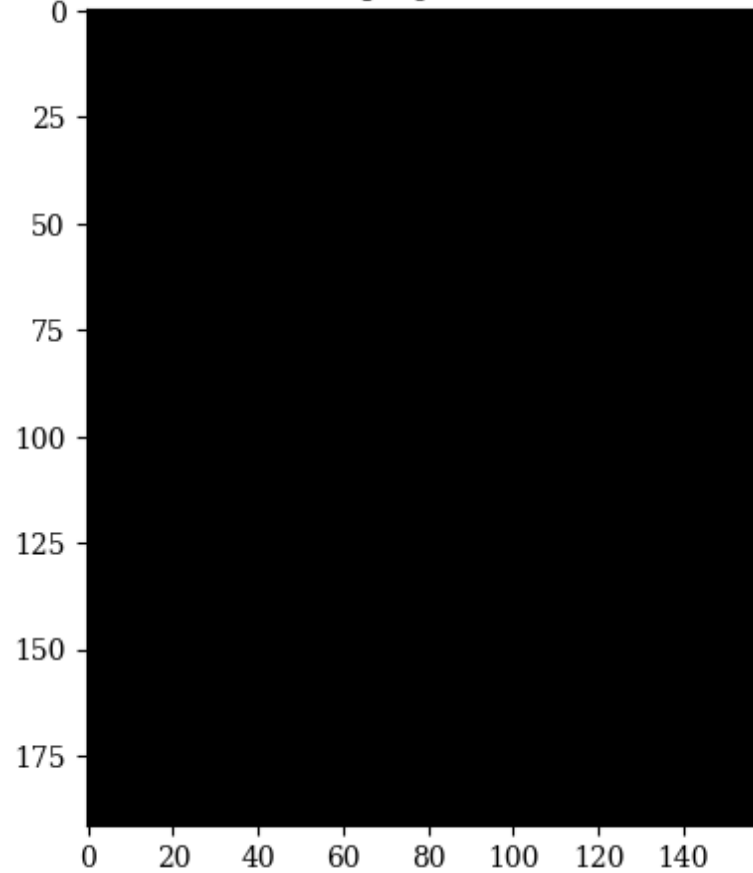
STEP 2: Validate full geometry simulations

Step 1: Background subtraction to isolate fluctuations

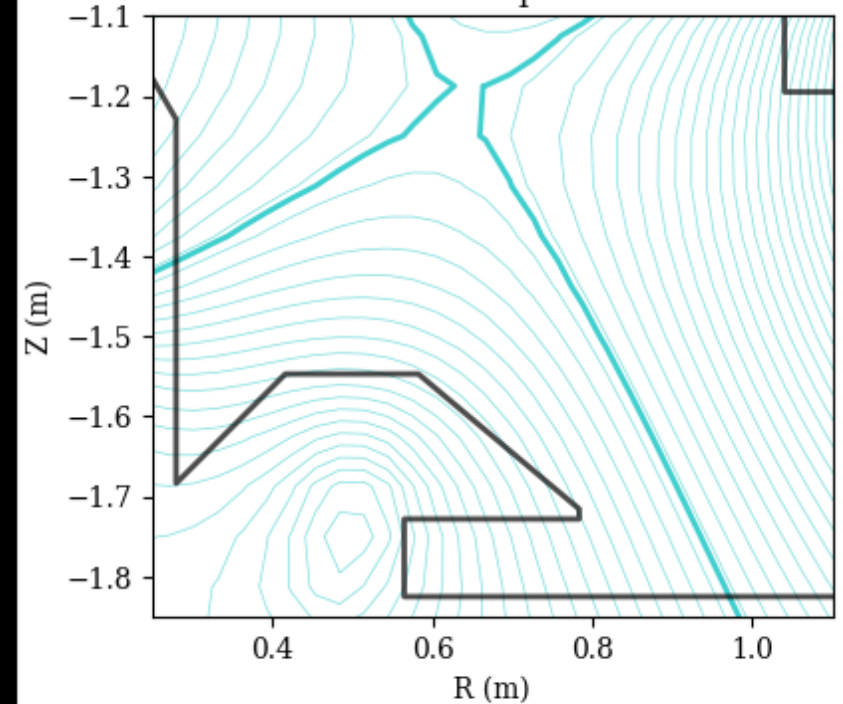
Camera frame



Reprojection



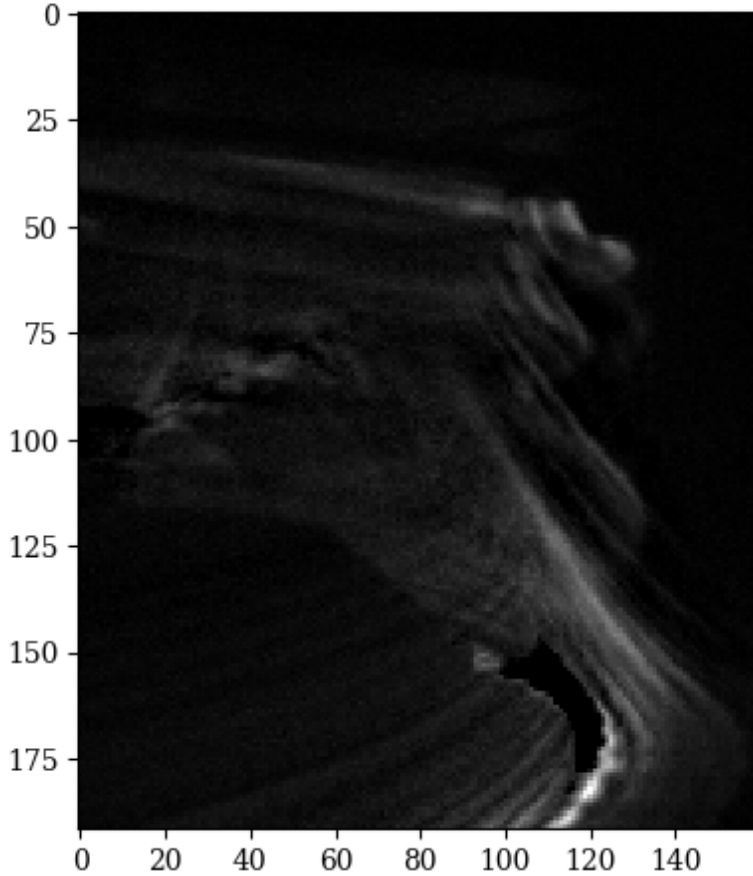
Poloidal plane



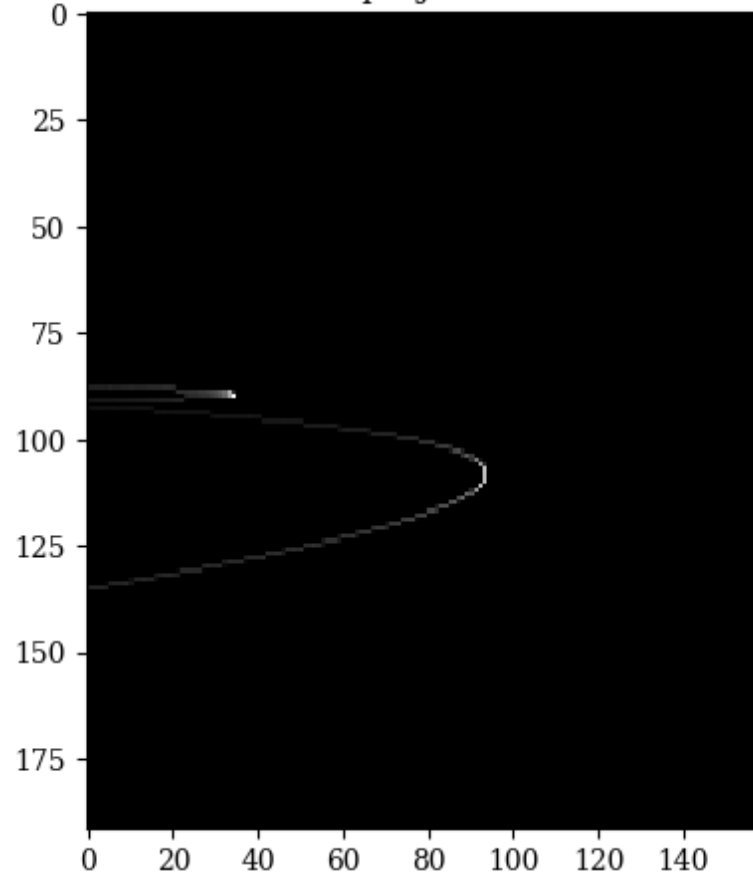
STEP 2: Validate full geometry simulations

Step 2: Project magnetic field lines onto camera image plane

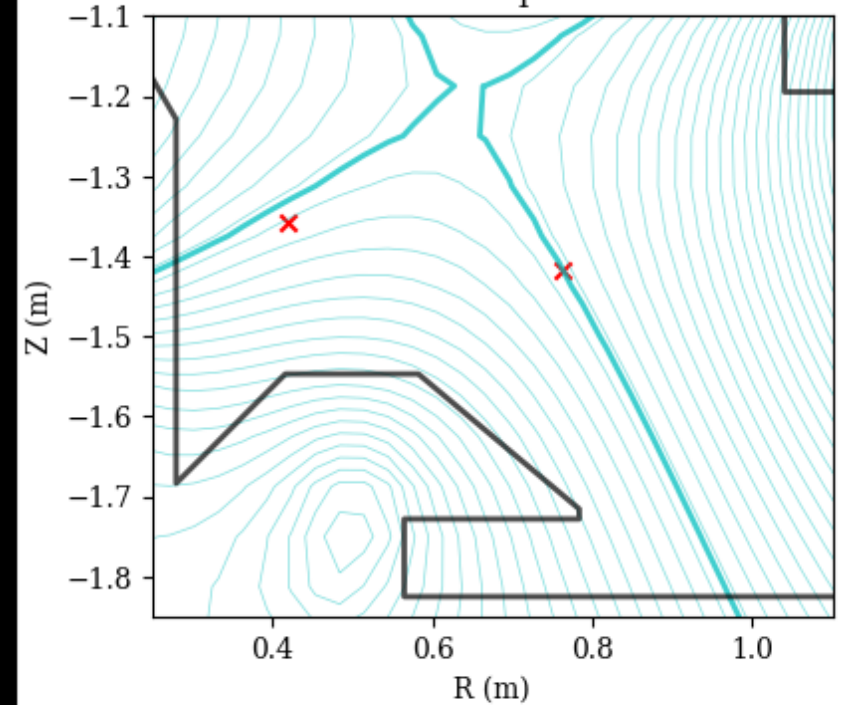
Camera frame



Reprojection



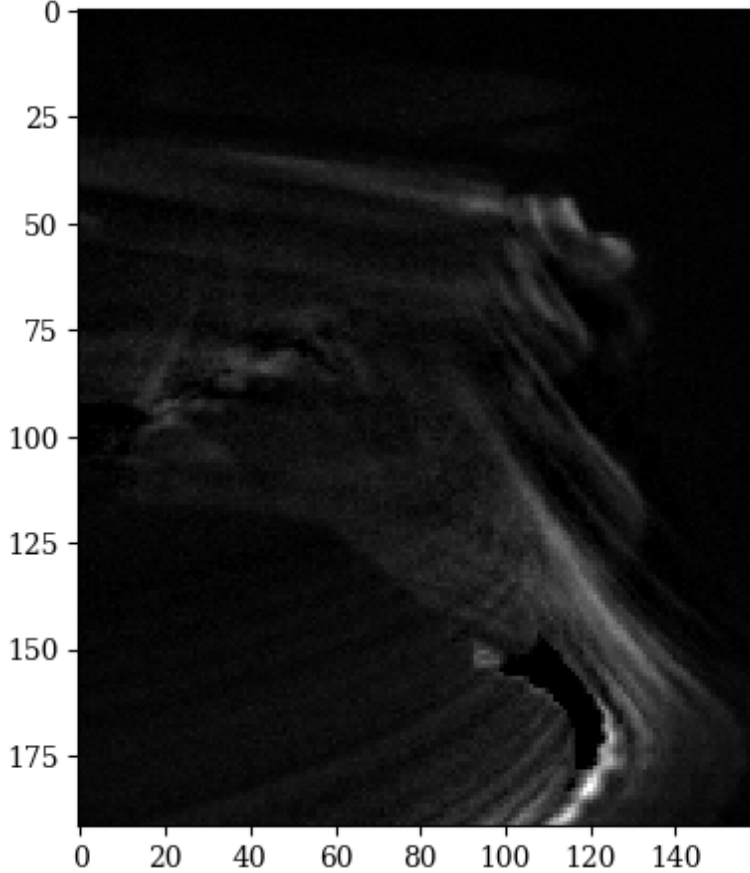
Poloidal plane



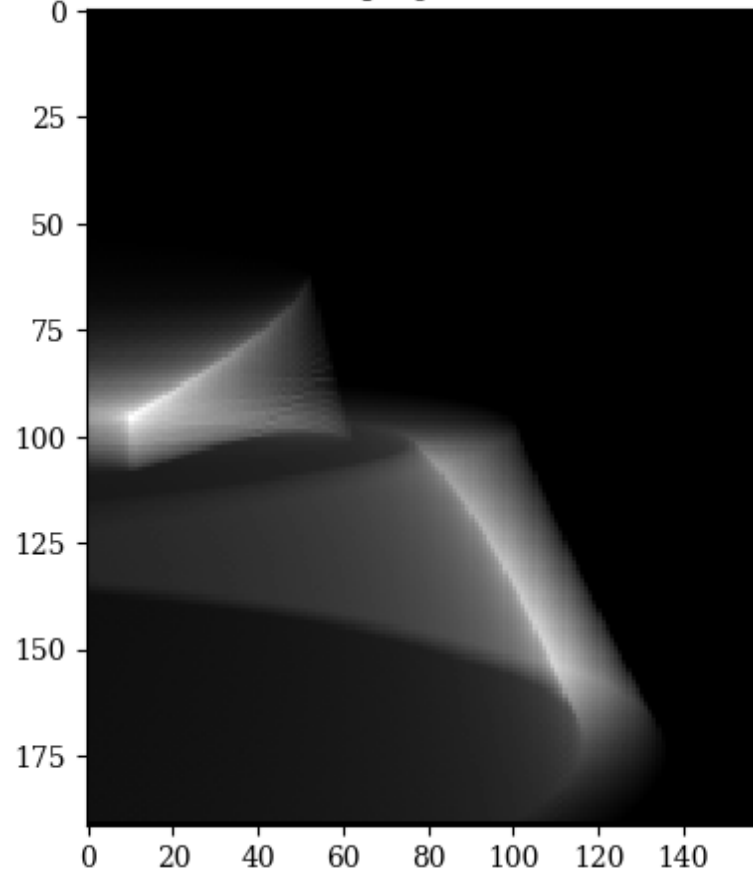
STEP 2: Validate full geometry simulations

Step 3: Create a basis-set of magnetic field lines

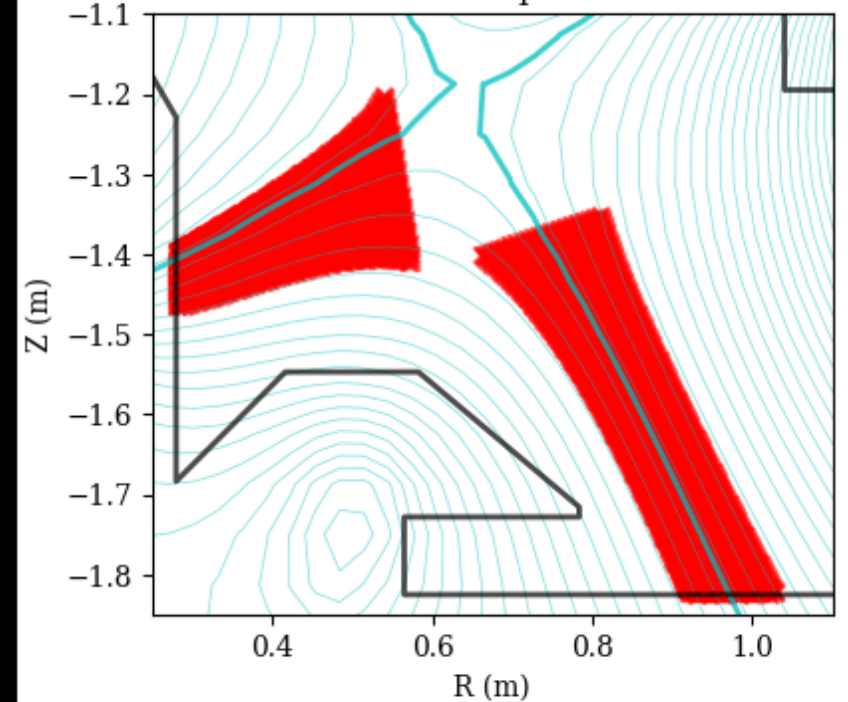
Camera frame



Reprojection



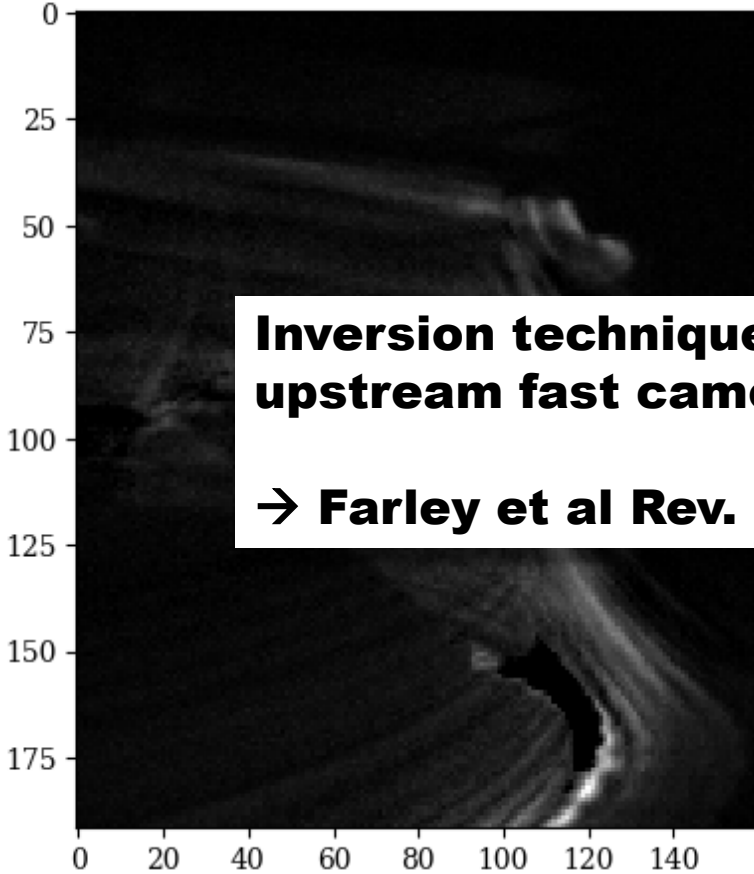
Poloidal plane



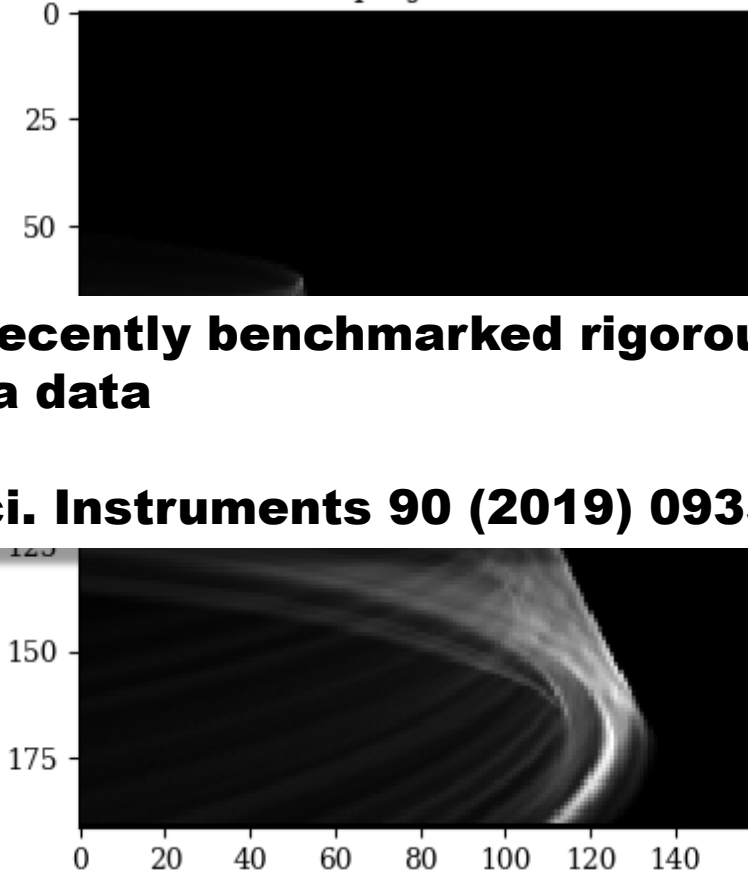
STEP 2: Validate full geometry simulations

Step 4: Find least-squares inversion of camera image onto basis-set

Camera frame



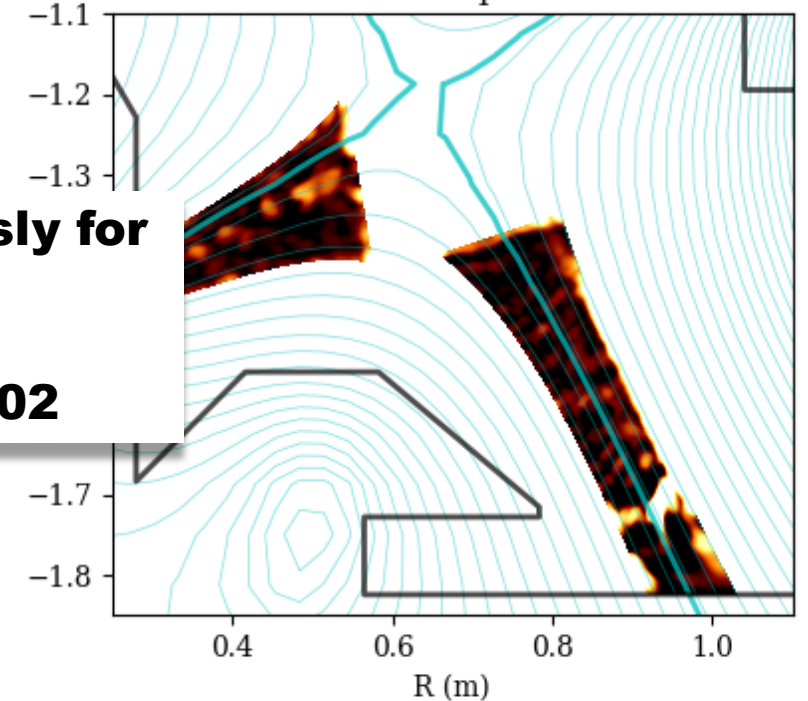
Reprojection



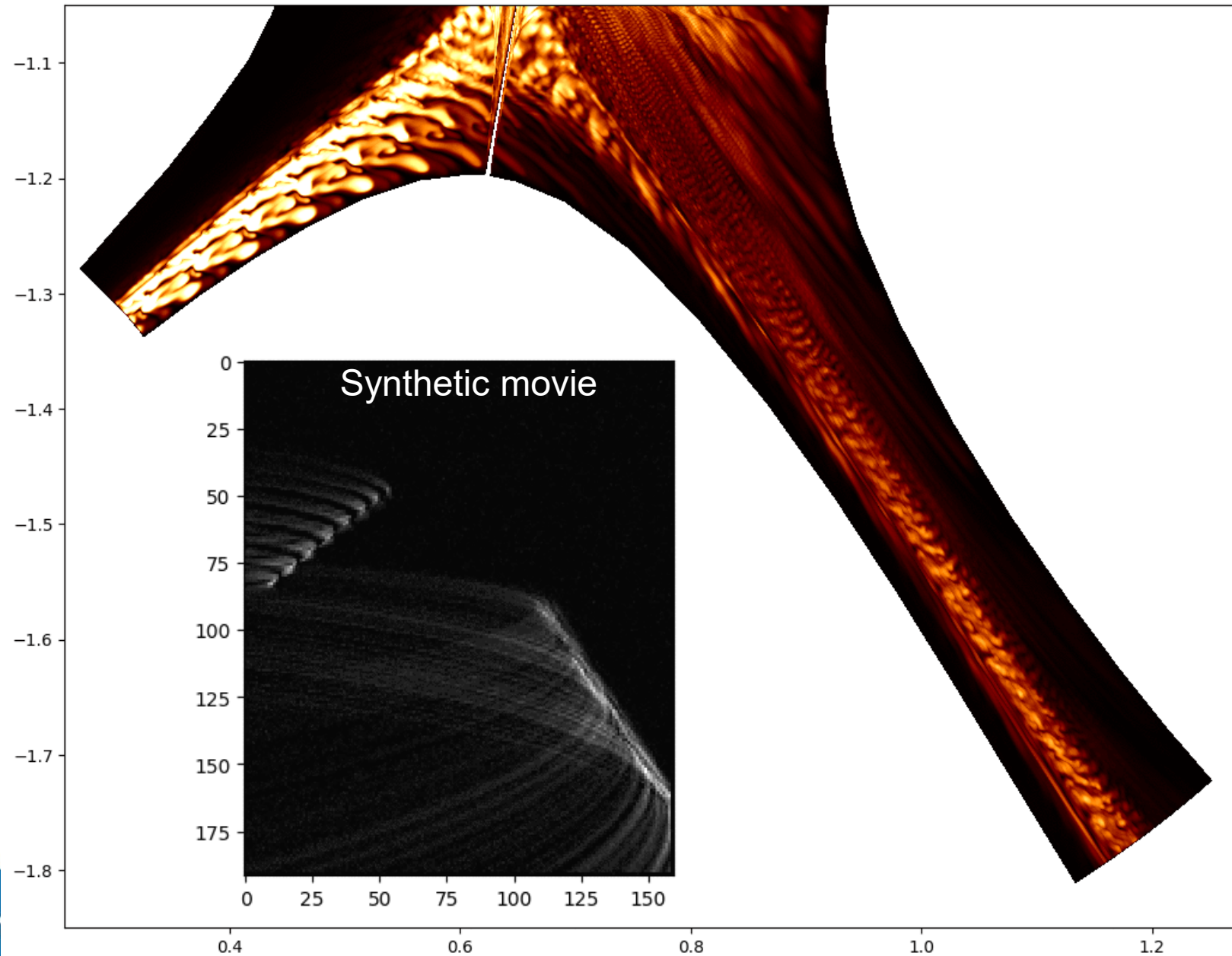
Inversion technique recently benchmarked rigorously for upstream fast camera data

→ Farley et al Rev. Sci. Instruments 90 (2019) 093502

Poloidal plane



STEP 2: Validate full geometry simulations



F.Riva *et al* Plasma Phys. Control.
Fusion **61** (2019) 094013

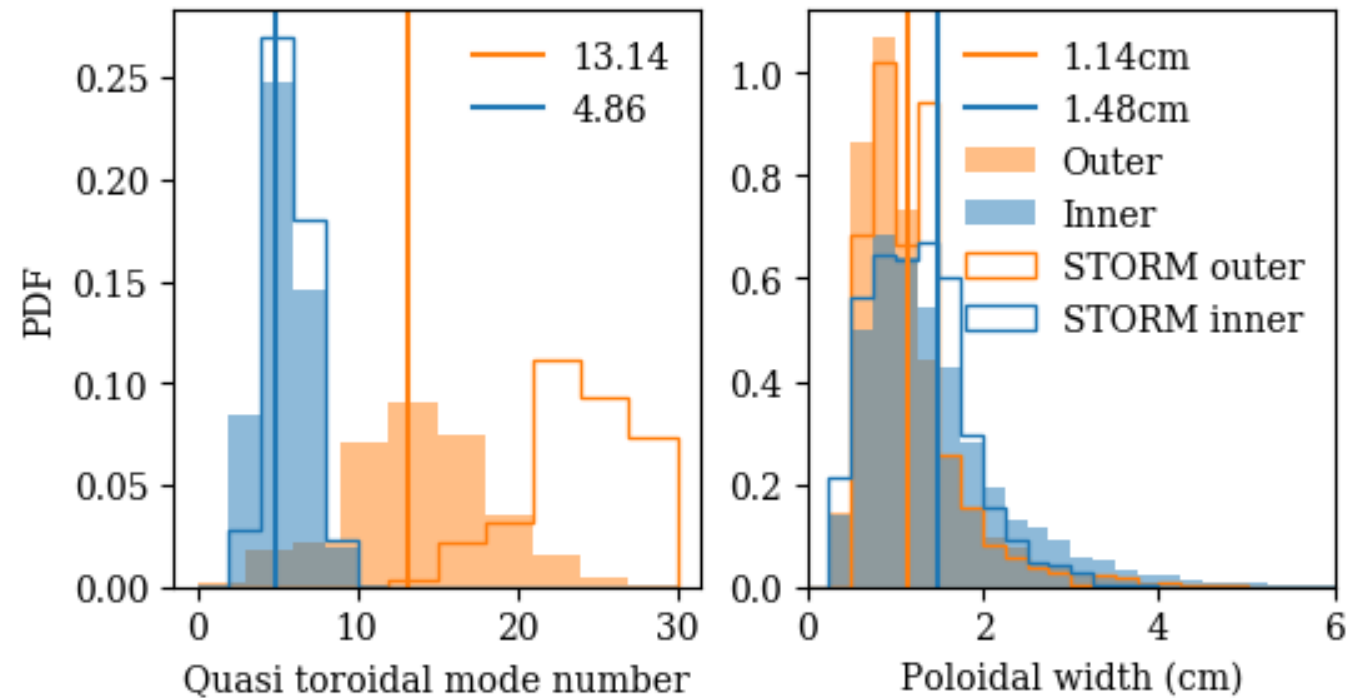
STEP 2: Validate full geometry simulations

Shot	Mode	$n_{e,sep}(10^{19}m^{-3})$	$T_{e,sep}(eV)$	$I_p(MA)$	$B_{tor}(T)$	$P_{NBI}(MW)$
29606	L-mode	0.72	18	0.63	-0.59	0
29608	L-mode	0.97	17	0.63	-0.57	0
29651	L-mode	0.85	24	0.62	-0.55	1.27
29660	L-mode (RMPs)	0.94	25	0.63	-0.54	1.22
29668	L-mode	1.05	27	0.63	-0.56	0.61
29669	L-mode	1.25	19	0.42	-0.51	0.62
29693	L-mode	0.97	32	0.42	-0.48	1.23
29718	L-mode	1.00	38	0.63	-0.54	1.61
29720	L-mode	1.37	29	0.42	-0.47	1.61
29723	H-mode (ELM-free)	1.4	55	0.82	-0.56	1.6
STORM [16]	L-mode	0.5	15	0.4	-0.4	0

STEP 2: Validate full geometry simulations

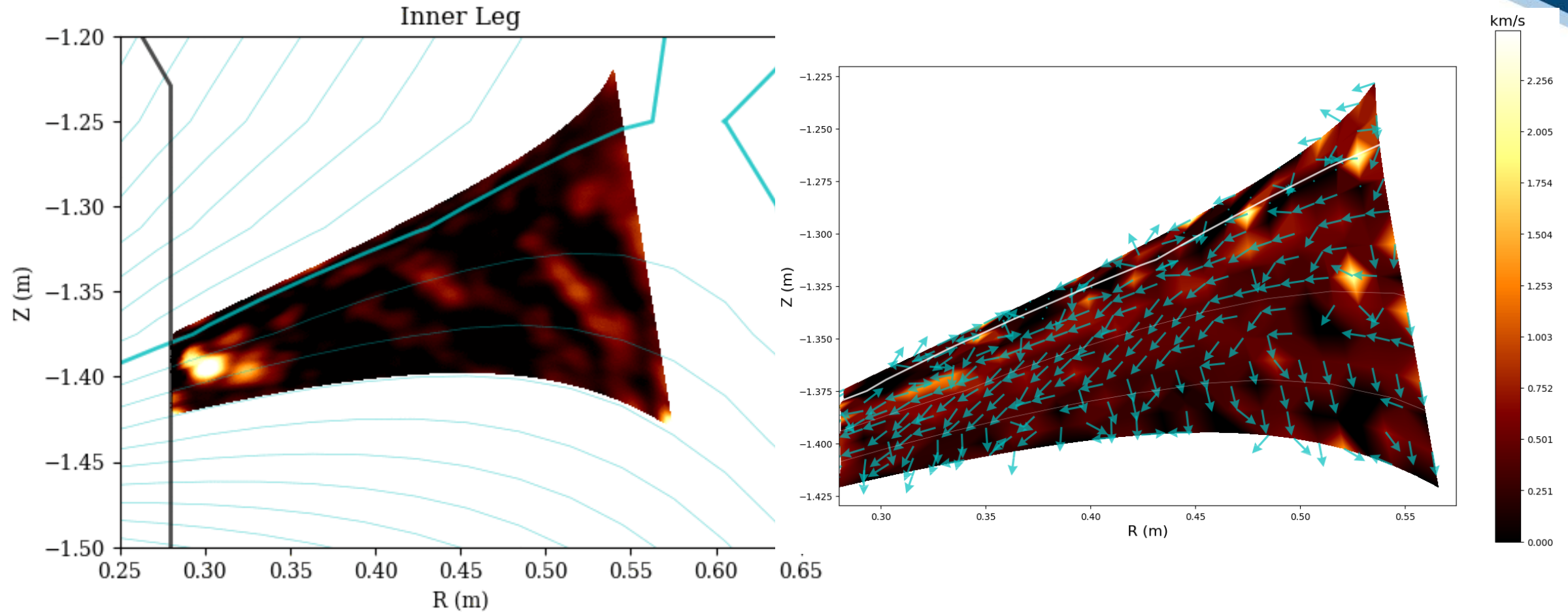
Measurements are made cumulatively across the shot database

- Inner and outer leg decoupled
- Similar poloidal sizes in both legs
- Strong collapse across database indicating insensitivity to operational parameters
- Excellent agreement from simulation, though over-estimation of outer-leg mode number



STEP 2: Validate full geometry simulations

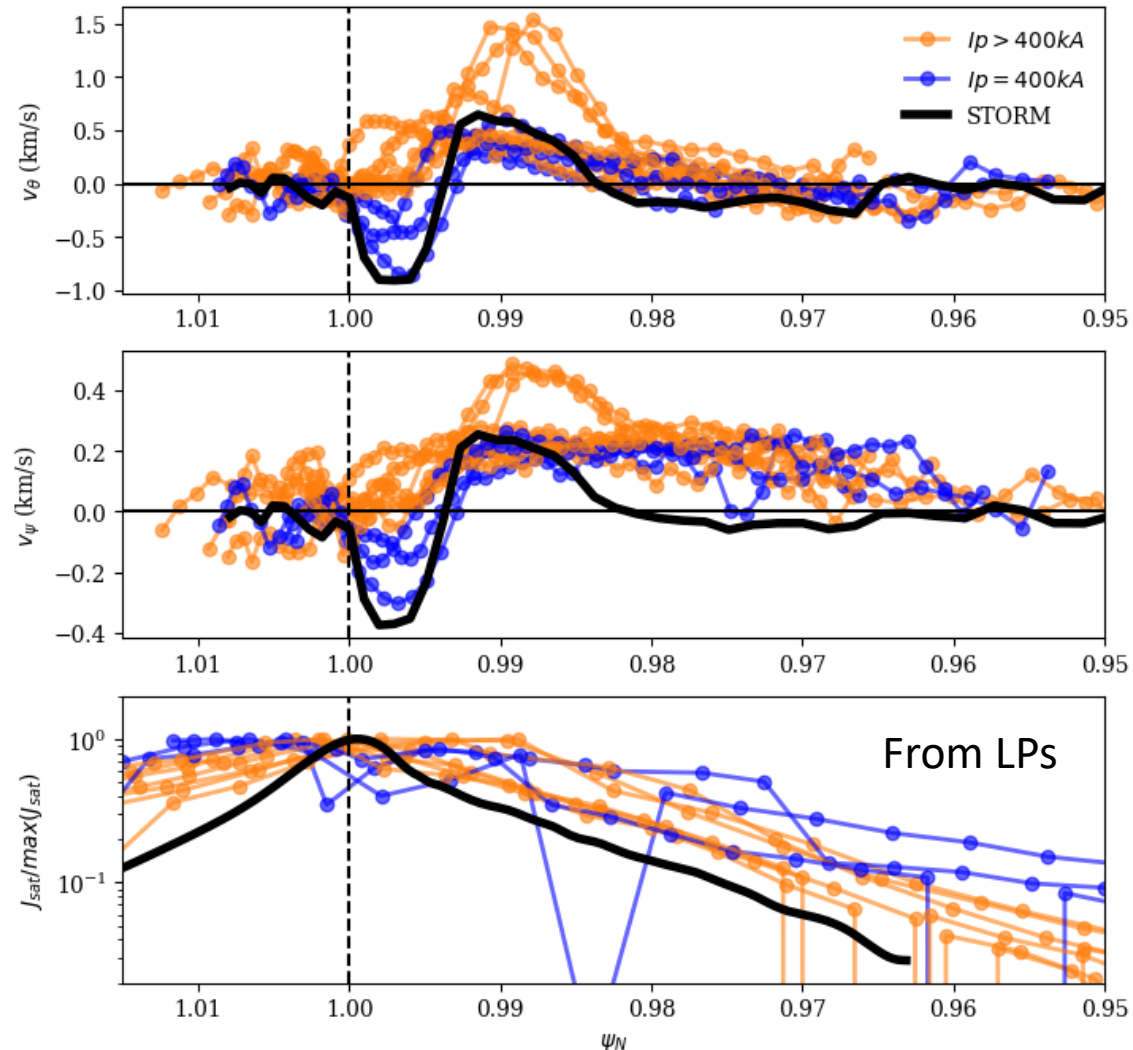
Two-point correlation technique used to map flow in inner divertor leg



STEP 2: Validate full geometry simulations

Two-point correlation technique used to map flow in inner divertor leg

- Broadly similar flow profiles, though some variation, particularly in poloidal flow
- Radial flow $\sim 200\text{m/s}$ in PFR concomitant with radial decay of J_{sat} at inner target
- Flow measurements from simulation match data extremely well, though radial velocity drops faster and profile decays quicker



STEP 3: Diagnose the turbulence

Impressive agreement between simulation and experiment means that simulations can be used to diagnose the turbulence

Vorticity eqn in STORM:

$$\frac{\partial \Omega}{\partial t} + U \mathbf{b} \cdot \nabla \Omega = -\mathbf{b} \times \nabla \phi \cdot \nabla \Omega + \frac{1}{n} \nabla \times \left(\frac{\mathbf{b}}{B} \right) \cdot \nabla P$$

$$+ \frac{1}{n} \nabla \cdot (\mathbf{b} J_{||}) + \mu_{\Omega_0} \nabla_{\perp}^2 \Omega$$

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Shear-flow turbulence
via Kelvin-Helmholtz
instability

$$+\frac{1}{n} \nabla \cdot (\mathbf{b} J_{||}) + \mu_{\Omega_0} \nabla_{\perp}^2 \Omega$$

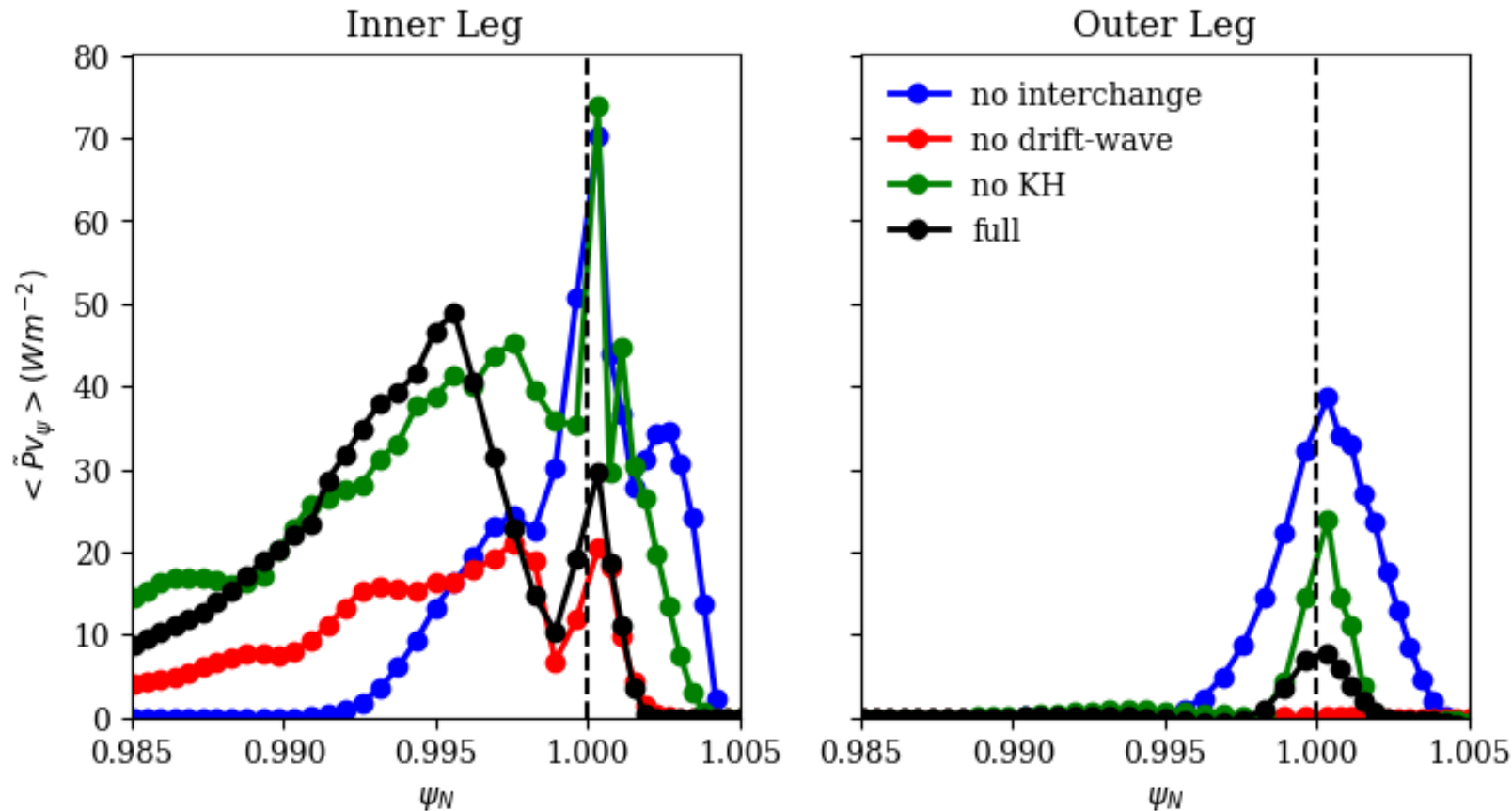
Drift-wave
turbulence

Curvature driven
turbulence via
interchange instability

STEP 3: Diagnose the turbulence

Impressive agreement between simulation and experiment means that simulations can be used to diagnose the turbulence

Removing these turbulence drives shows how each contributes to the total radial fluxes



- Generally higher and more radially extended fluxes in inner leg than outer
- Shear-flow (KH) effects are stabilizing in both divertor legs
- Inner-leg turbulence is drift-interchange
- Outer-leg turbulence is drift-wave with curvature playing a stabilizing role

What is divertor turbulence, and why is it important?

Can we *understand* divertor turbulence?

Summary

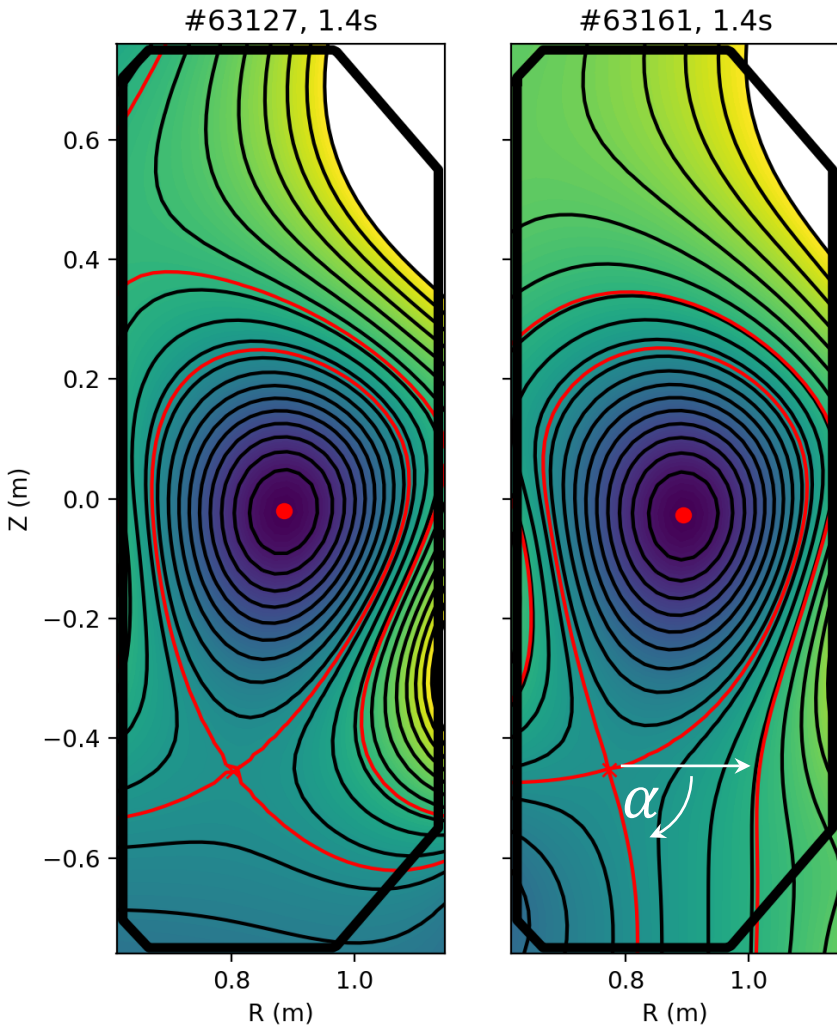
Summary

1. Radial transport in the divertor is a complex non-linear turbulent phenomenon
2. Divertor turbulence is relatively insensitive to parameters of the plasma
3. Turbulence in the two divertor legs differs significantly
 - On the inner divertor leg turbulence is mainly interchange
 - On the outer leg, turbulence is mainly drift-wave
4. The magnetic curvature plays a vital role in divertor turbulence
 - It drives transport into the PFR in the inner leg
 - It suppresses transport into the PFR in the outer leg

This is just the start, there is a lot of learning to go!

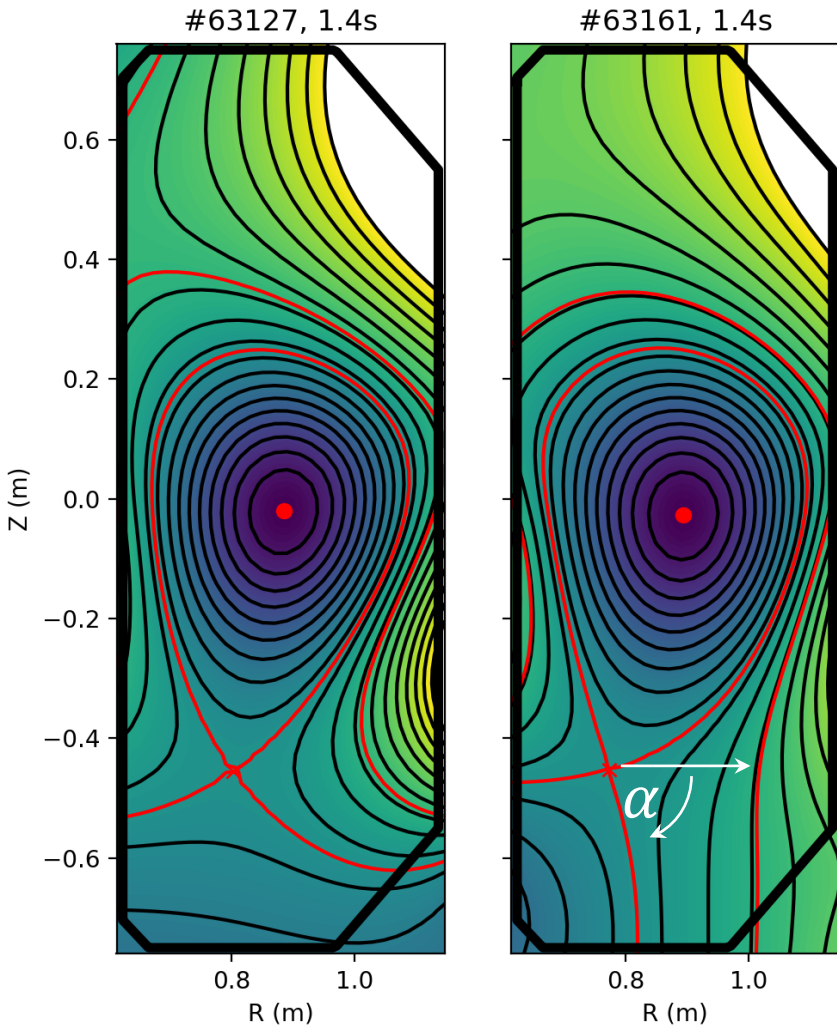
STEP 4: Test the conclusions via experiment

Aim: Test in impact of the magnetic curvature by varying the poloidal divertor leg angle



STEP 4: Test the conclusions via experiment

Aim: Test in impact of the magnetic curvature by varying the poloidal divertor leg angle



$$\alpha \approx -\arctan\left(\frac{Z_{SP} - Z_X}{R_{SP} - R_X}\right)$$

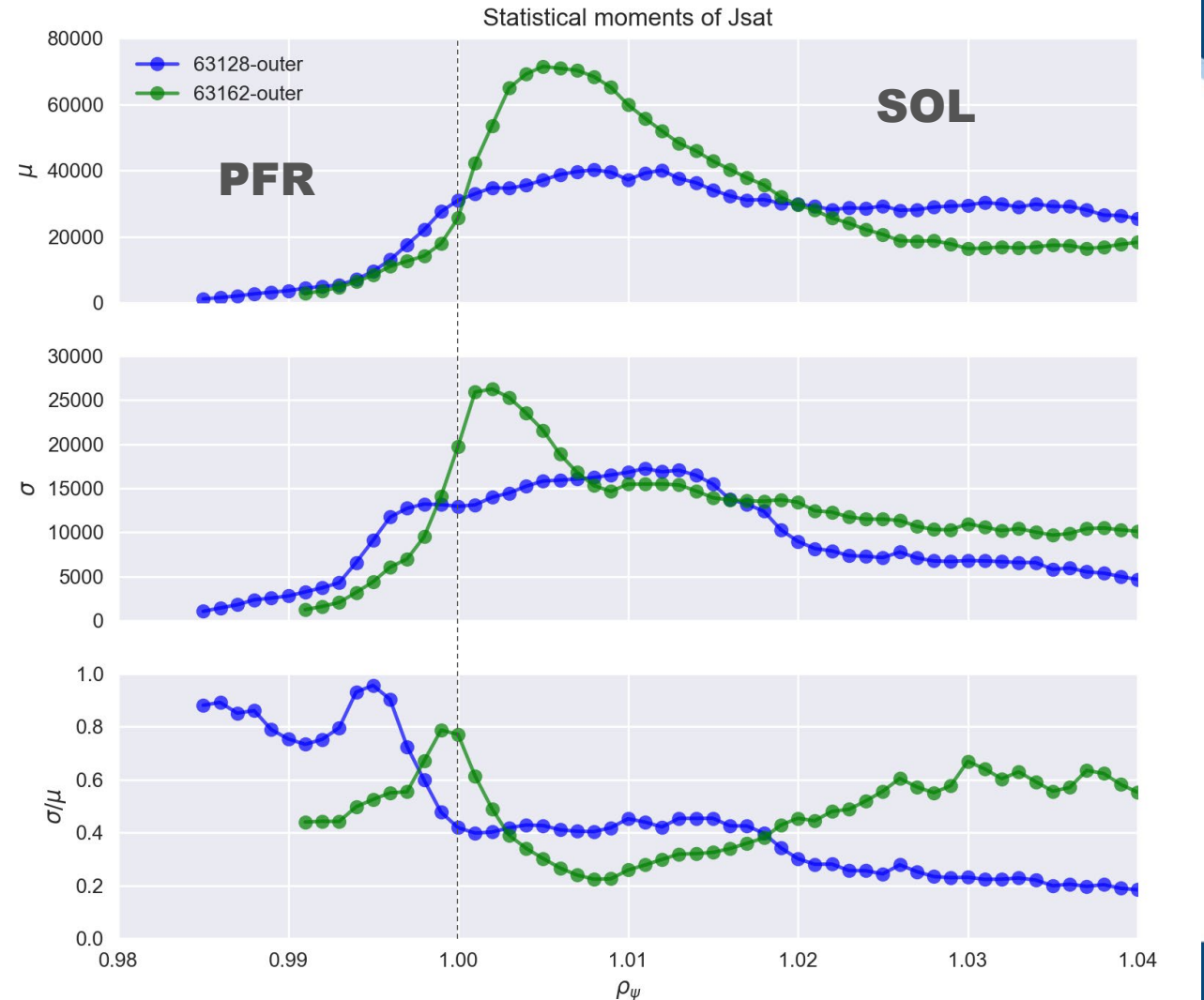
Shot	63127/28	63161/62
α (deg)	32	80

STEP 4: Test the conclusions via experiment

Clear change in profiles at the outer target

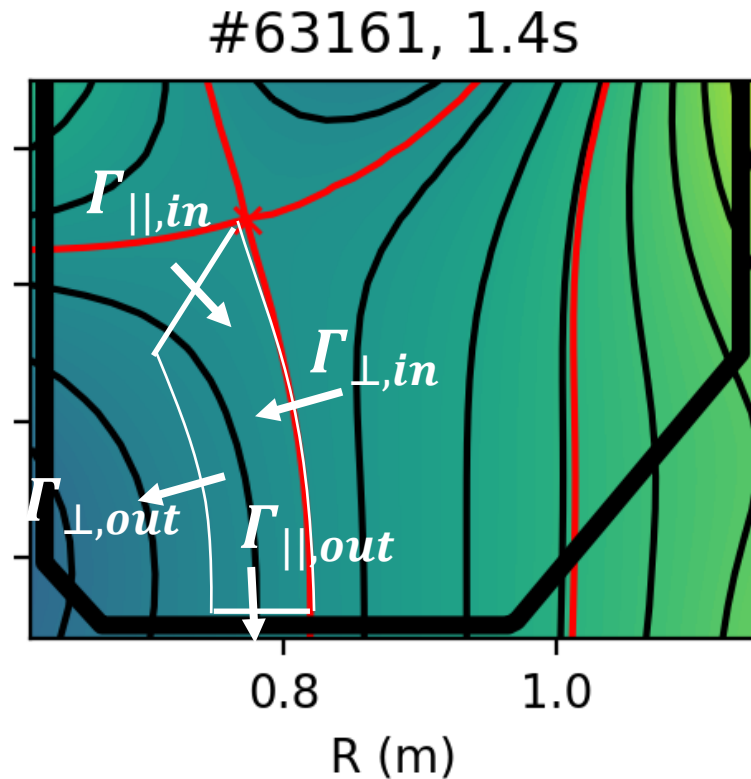
The horizontal leg shows

- Increased spreading into the PFR
- Generally flatter profile
- Higher standard deviation in the PFR
- 50% higher fluctuation level in the PFR
- Peak in fluctuation level further into PFR



STEP 4: Test the conclusions via experiment

Treating the PFR as a closed system with no sources we can estimate a poloidally averaged radial transport flux

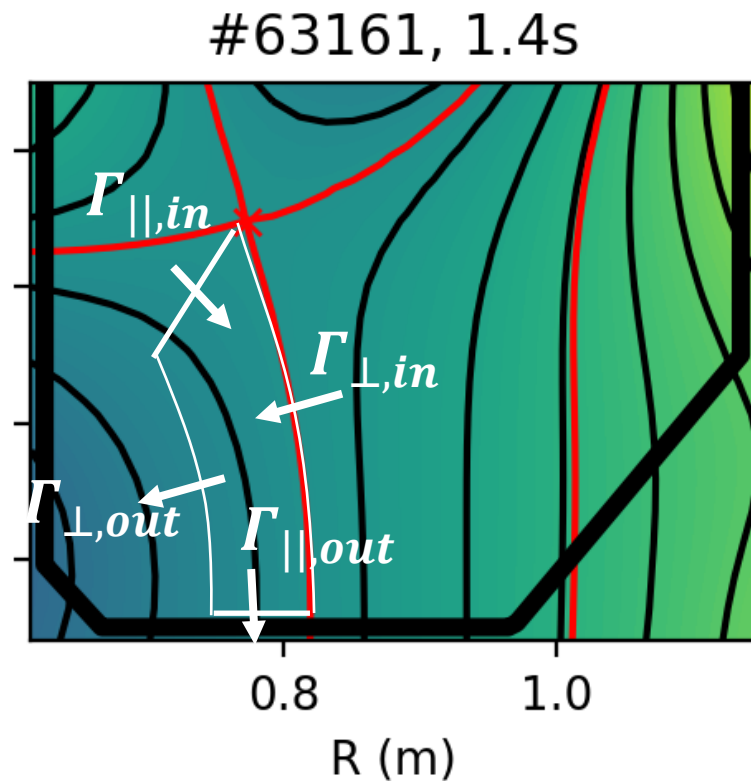


STEP 4: Test the conclusions via experiment

Treating the PFR as a closed system with no sources we can estimate a poloidally averaged radial transport flux

Assume:

- Stagnation near the X-point $\rightarrow \Gamma_{\parallel,in} = 0$
- Outer PFR sufficiently far from separatrix $\rightarrow \Gamma_{\perp,out} = 0$

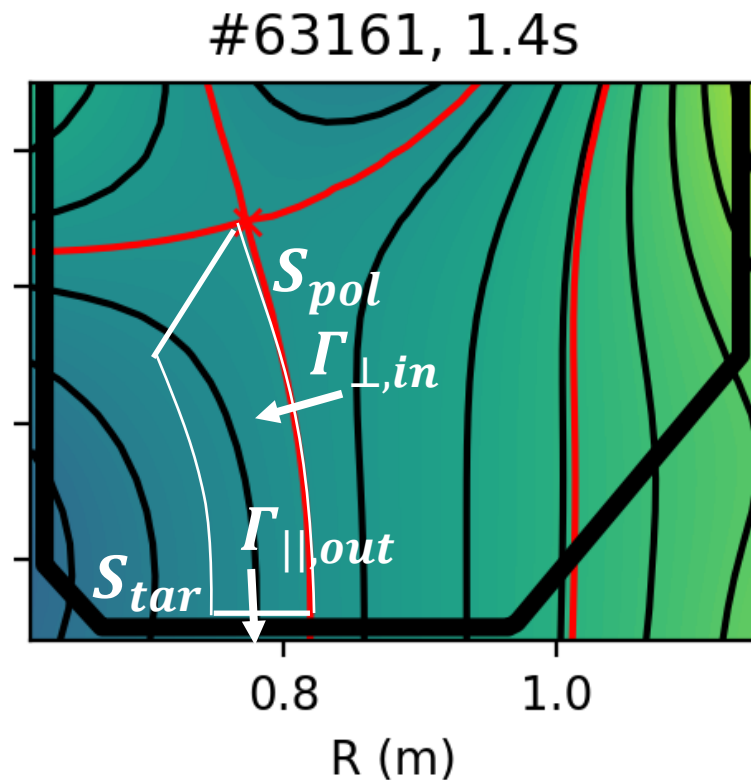


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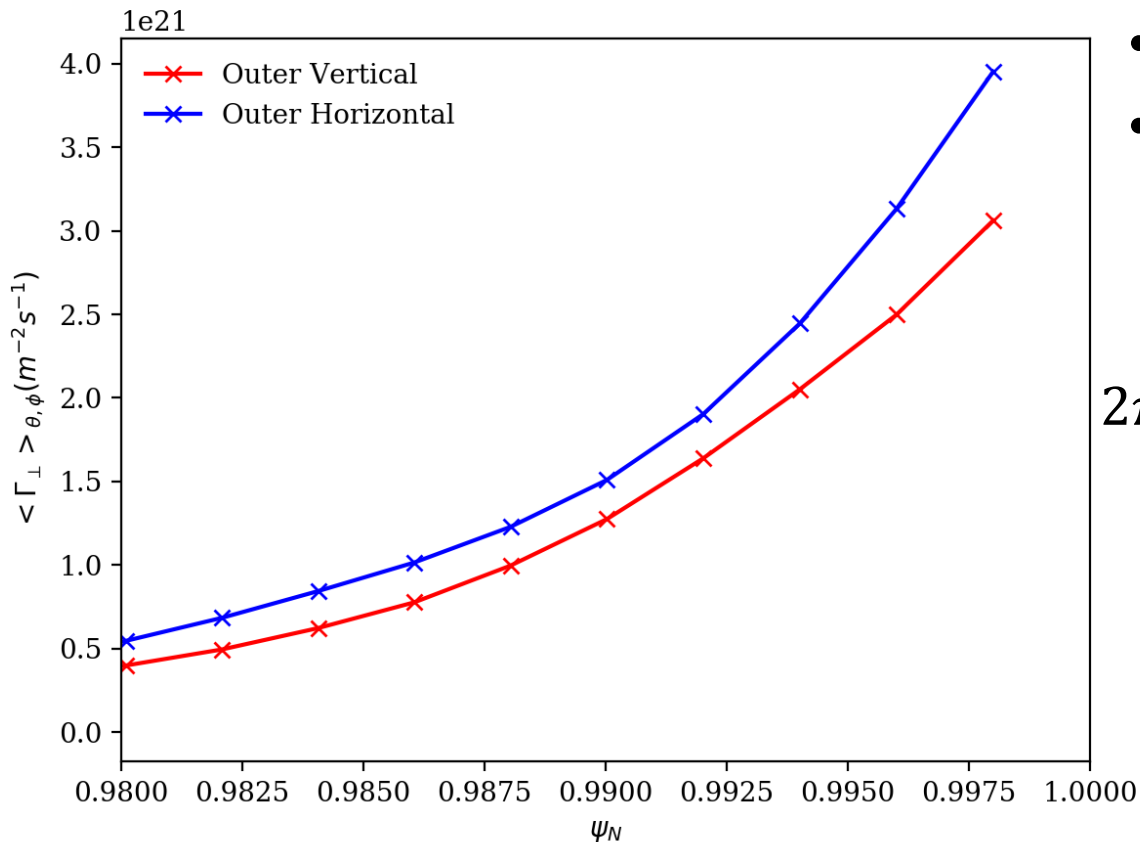


$$2\pi \int \Gamma_{\perp} R(S_{pol}) dS_{pol} = 2\pi \int \Gamma_{\parallel} \frac{B_{pol}(S_{tar})}{B(S_{tar})} R(S_{tar}) dS_{tar}$$

$$\langle \Gamma_{\perp} \rangle \approx \frac{\int \Gamma_{\parallel} \frac{B_{pol}(S_{tar})}{B(S_{tar})} R(S_{tar}) dS_{tar}}{\int R(S_{pol}) dS_{pol}}$$

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$$2\pi \int \Gamma_{\perp} R(S_{pol}) dS_{pol} = 2\pi \int \Gamma_{\parallel} \frac{B_{pol}(S_{tar})}{B(S_{tar})} R(S_{tar}) dS_{tar}$$

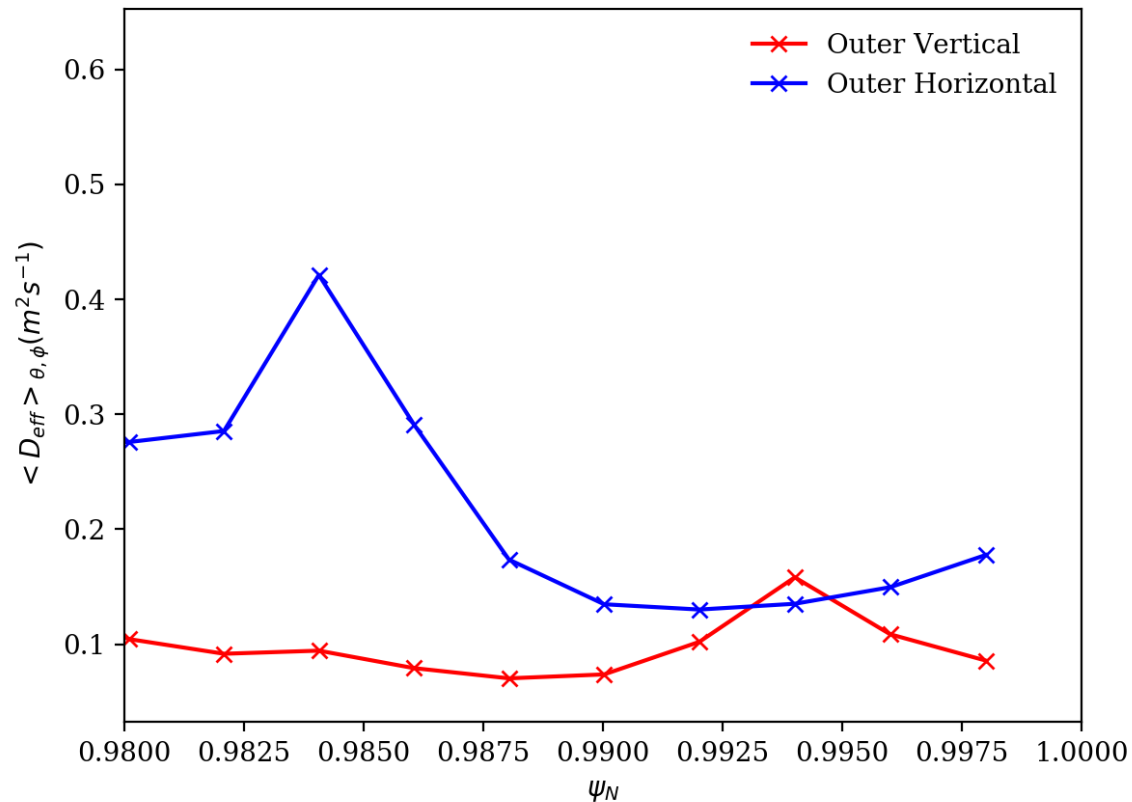
$$\langle \Gamma_{\perp} \rangle \approx \frac{\int \Gamma_{\parallel} \frac{B_{pol}(S_{tar})}{B(S_{tar})} R(S_{tar}) dS_{tar}}{\int R(S_{pol}) dS_{pol}}$$

STEP 4: Test the conclusions via experiment

Treating the PFR as a closed system with no sources we can estimate a poloidally averaged radial transport flux

Assume:

- Stagnation near the X-point $\rightarrow \Gamma_{\parallel, in} = 0$
- Outer PFR sufficiently far from separatrix $\rightarrow \Gamma_{\perp, out} = 0$
- Density profile can be inferred from Jsat profile scaled by peak target density
- Transport can be expressed as a diffusion or convection



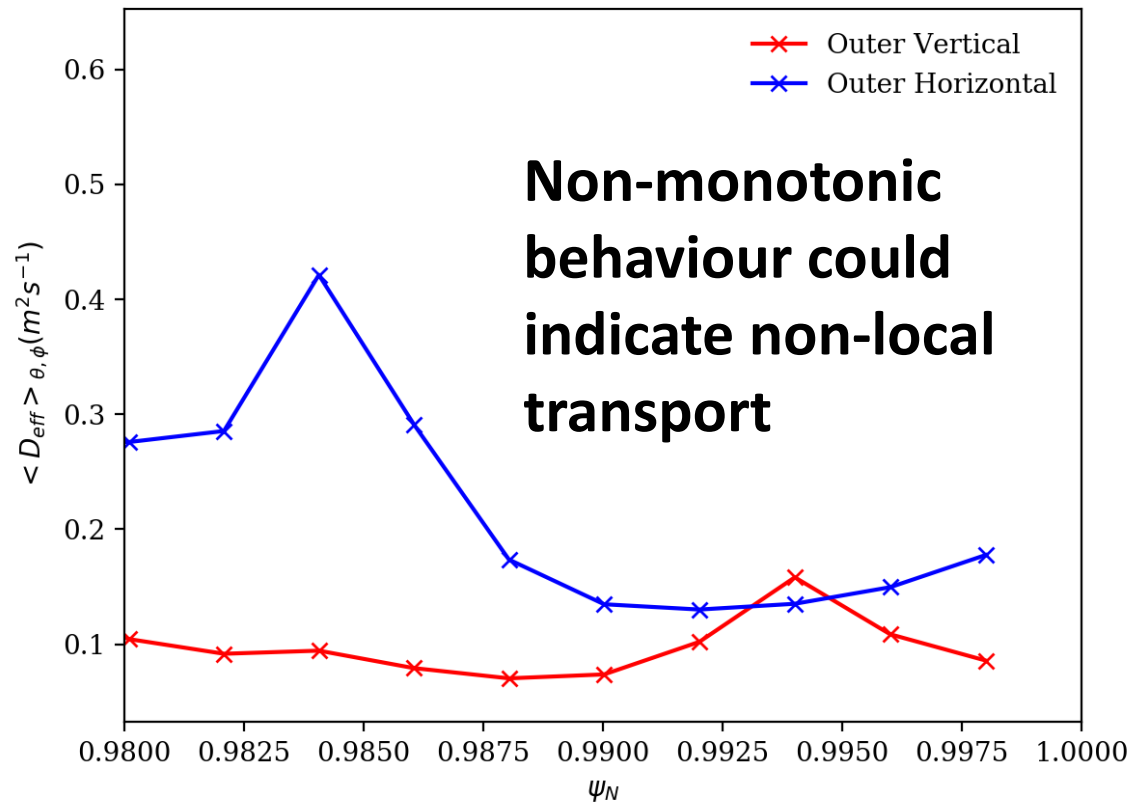
$$\langle D_{\perp} \rangle \approx \frac{\int \Gamma_{\parallel} \frac{B_{pol}(S_{tar})}{B(S_{tar})} R(S_{tar}) dS_{tar}}{\frac{\partial n}{\partial \psi} \int B_{pol}^{-1}(S_{pol}) dS_{pol}}$$

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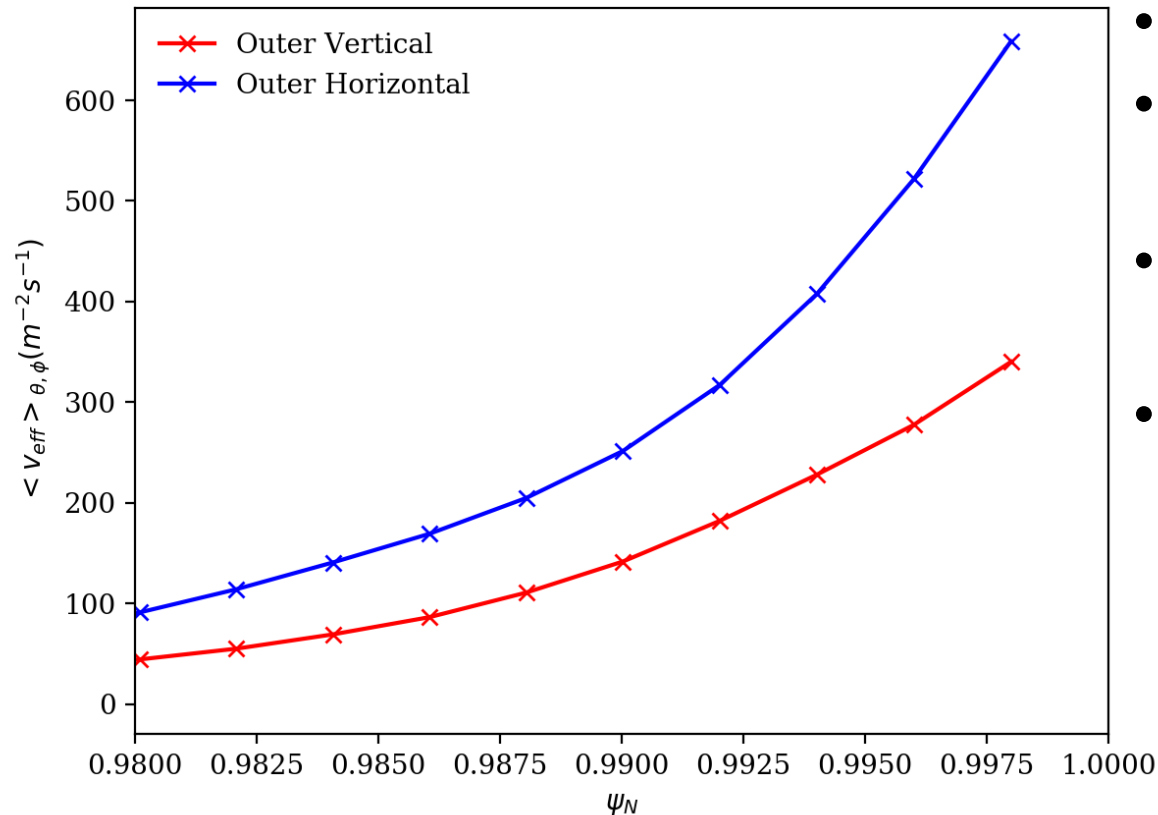
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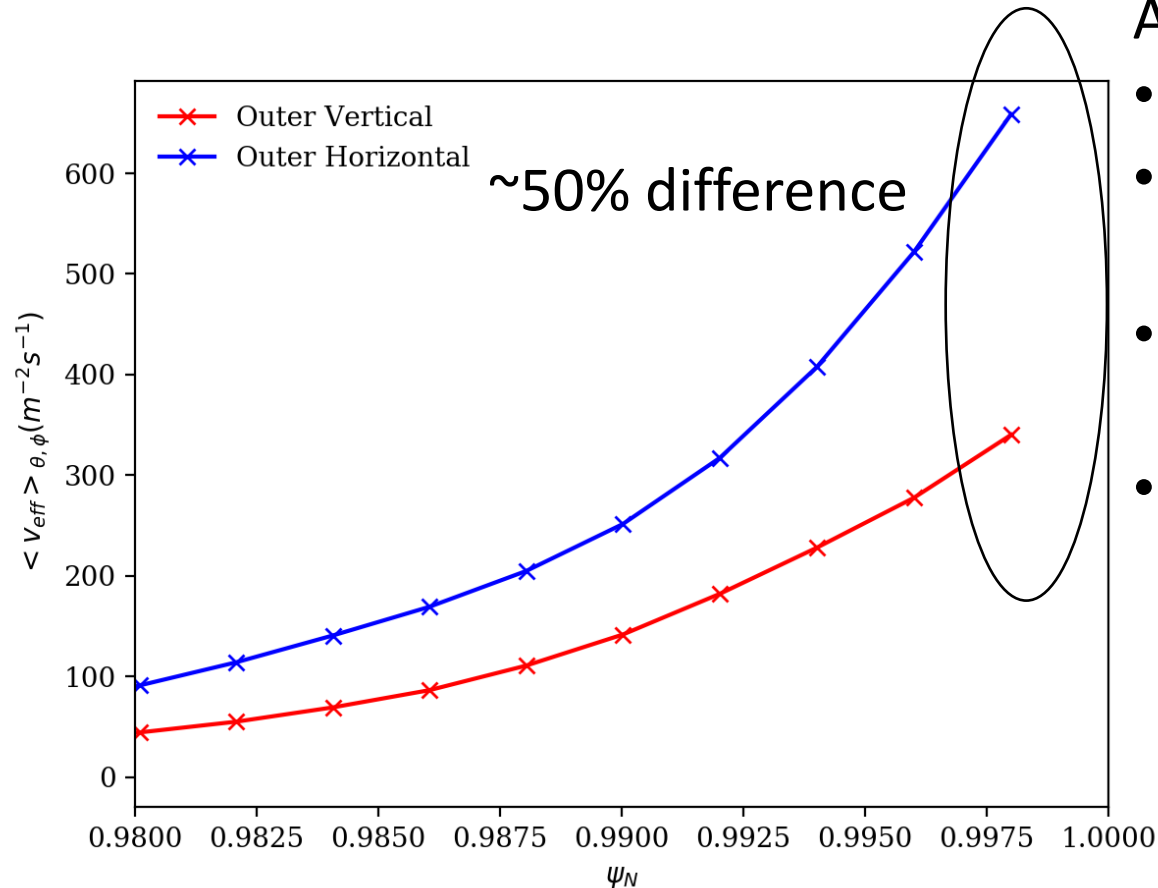
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